Cranston, Rhode Island Knights Corner Development

April 2023

TRAFFIC IMPACT STUDY





Proposed Mixed-Use Development Knights Corner Cranston, Rhode Island

TRAFFIC IMPACT STUDY

- Prepared by: BETA GROUP, INC.
- Prepared for: 333 Main Street, LLC 201 Lippitt Avenue Cranston, Rhode Island 02921

April 2023



April 7, 2023

Mr. Jotham Coe 333 Main Street, LLC 201 Lippitt Avenue Cranston, Rhode Island 02921

Re: Proposed Mixed Use Development Knights Corner Cranston, Rhode Island

Dear Mr. Coe:

BETA Group, Inc., in accordance with our scope of services, has completed a traffic impact study for a proposed mixed-use development project in the City of Cranston, Rhode Island. The site is situated on a parcel of land on the southwest corner of the intersection of Cranston Street with Dyer Avenue, abutting the Cranston Fire Department Station 3 to the east. The parcel is defined by Assessor's Plat 8, Lots 203 and 2739, which together contain approximately 4.72 acres of partially developed land that contains an historic church building and associated parking lot.

Based upon our discussions with the site engineer and a review of the conceptual plans provided by *DiPrete Engineering* it is our understanding that the property will be developed to include construction of four new buildings containing residential apartments. In addition, the historical *Sprague Meeting House* church building will be renovated for a fine dining restaurant use. Access/egress to the site is proposed via three driveways, two of which to be located on Cranston Street and one located on Dyer Avenue.

The study included herein, was conducted to determine the adequacy of the existing servicing roadways to accommodate anticipated traffic to be generated by the mixed-use development project. An analysis of potential impacts to the roadway capacity and safety has been completed and is discussed in the following report.

Very truly yours, BETA Group, Inc.

Paul J. Bannon Associate

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SBETA

1.0 INTRODUCTION

The objective of the following study is to assess the potential traffic impacts associated with a proposed mixed-use development project in the City of Cranston, Rhode Island. The property is located in the *Knightsville* section of the city with frontage on both Cranston Street and Dyer Avenue. Refer to Figure 1 on the following page for the project location within the city. The property is comprised of approximately five acres of partially developed land containing a single building and associated paved parking lot. The small historical building known as the *Sprague Meeting House* was constructed in the early 1800's and moved to its current location in 1864. It was used as an Episcopal church for the small village community that was built, along with housing and other amenities, around the *Print Works* textile mill that was owned by the Sprague family during the 1800's. The mill complex which is situated to the immediate north of the subject property, closed their manufacturing operation over two decades ago, but the corporate office remains on site, though there is a current proposal to redevelop the property.

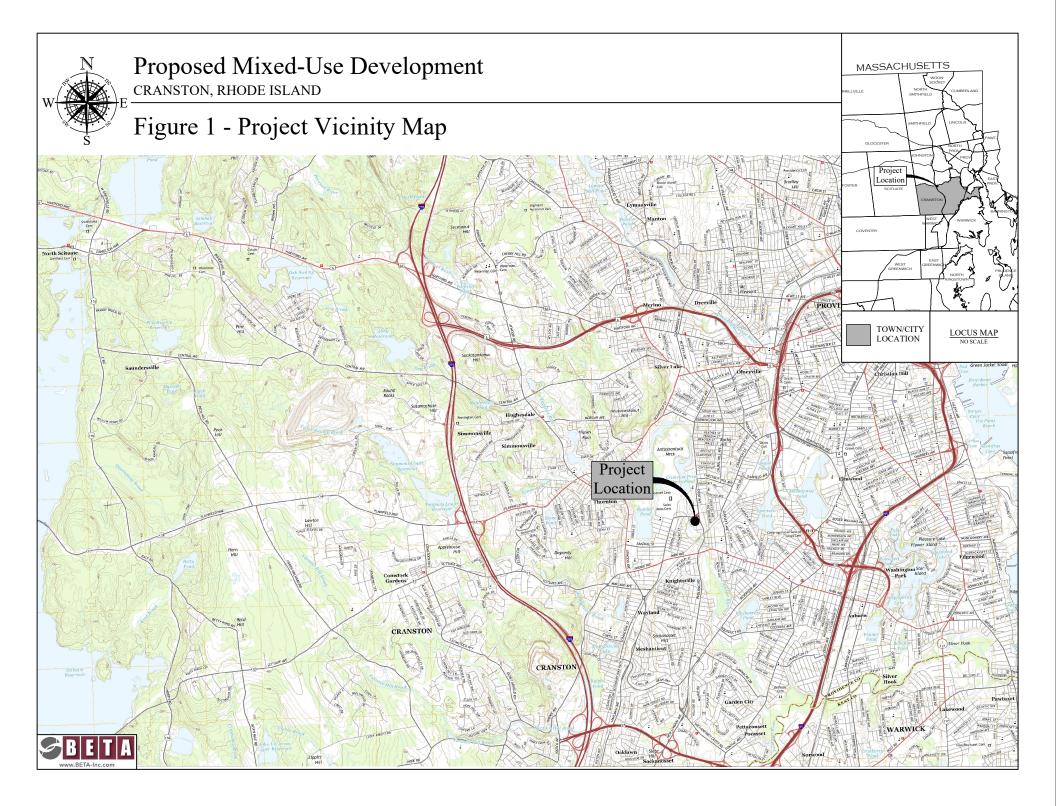
Development of the 4.72 acre subject property will include renovation of the existing historic church building to accommodate a fine dining restaurant containing approximately 96 seats. The remainder of the property will be developed for residential apartment use in four new buildings containing 156 residential units. A total of 266 parking spaces will be provided in both surface lots and in structured garage parking on the first level of the apartment buildings. Access/egress to the parking areas are proposed from Cranston Street via two driveways approximately 260 feet to the west of the intersection with Dyer Avenue, and one proposed driveway along Dyer Avenue, approximately 460 feet south of the intersection with Cranston Street.

The study summarized herein focused on both traffic flow efficiency and safety along Cranston Street and Dyer Avenue within the immediate vicinity of the subject property, specifically including their junction and the new site driveways. The potential impacts associated with the site related traffic have been defined and evaluated in accordance with standard traffic engineering guidelines and procedures.

The traffic engineering study completed for this project included the following:

- A traffic counting program to define the existing traffic patterns and operational characteristics along the servicing roadways. The data collection included an Automatic Traffic Recorder (ATR) count on Dyer Avenue, a manual Turning Movement Counts (TMC) at the intersection of Cranston Street with Dyer Avenue, review of record volume data from the Rhode Island Department of Transportation and from a recent study completed in the project area.
- An inventory of the physical roadway characteristics of Cranston Street and Dyer Avenue to determine the adequacy of the existing roadway geometric features in reference to safety and operations.
- An analysis of crash records obtained from the Cranston Police Department to determine if there are any safety concerns relative to the frequency, severity, or pattern of crashes in the project area.





- An estimate of future traffic volumes for the proposed mixed-use development was calculated using data from the "Trip Generation" Manual, an informational report published by the Institute of Transportation Engineers (ITE).
- Evaluation and analysis of the traffic safety and operational issues for existing and future traffic conditions.
- Development of recommendations where necessary, that would be required to maintain safe and efficient traffic flow in the project area.

2.0 PROJECT AREA

As noted in the previous section, the proposed *Knights Corner* development is situated on a parcel of land along the southerly side of Cranston Street to the immediate west of Cranston Fire Department Station 3. The property also has approximately 55 feet of frontage on Dyer Avenue located 460 feet south of Cranston Street. The 4.72 acre site is primarily undeveloped and wooded in the southern and eastern portions of the lot, though as previously noted, is developed along the Cranston Street frontage with the historic church building and associated paved parking lot. Figure 2 on the following page depicts the general project area, and the boundary lines of the subject property.

Land use in the immediate area can be defined as a mixture of commercial and residential properties along Cranston Street and Dyer Avenue, with high density residential neighborhoods located off of intersecting side streets. Within the village area of Dyer Avenue to the north are multi-unit residential homes that were built for housing to support the large textile manufacturing operation at the *Cranston Print Works* mill site to the immediate north. The Sprague Mansion, an historical museum is situated on the northeast corner of the intersection. Commercial properties dominate the frontage of Dyer Avenue heading south to Park Avenue (Route 12). Further west heading into the village, is the Saint Ann catholic church and cemetery.

Both Cranston Street and Dyer Avenue will serve as the primary access routes to the proposed development. Based upon the good operating characteristics along the servicing roadways, and the minor estimated hourly volume and type of traffic associated with the proposal, a study impact area was defined for the project. The limits of our analysis focused on Dyer Avenue between Industrial Road and Governor Street and Cranston Street between Byron Street and Florida Avenue, and specifically the signalized junction of these two major roadways.

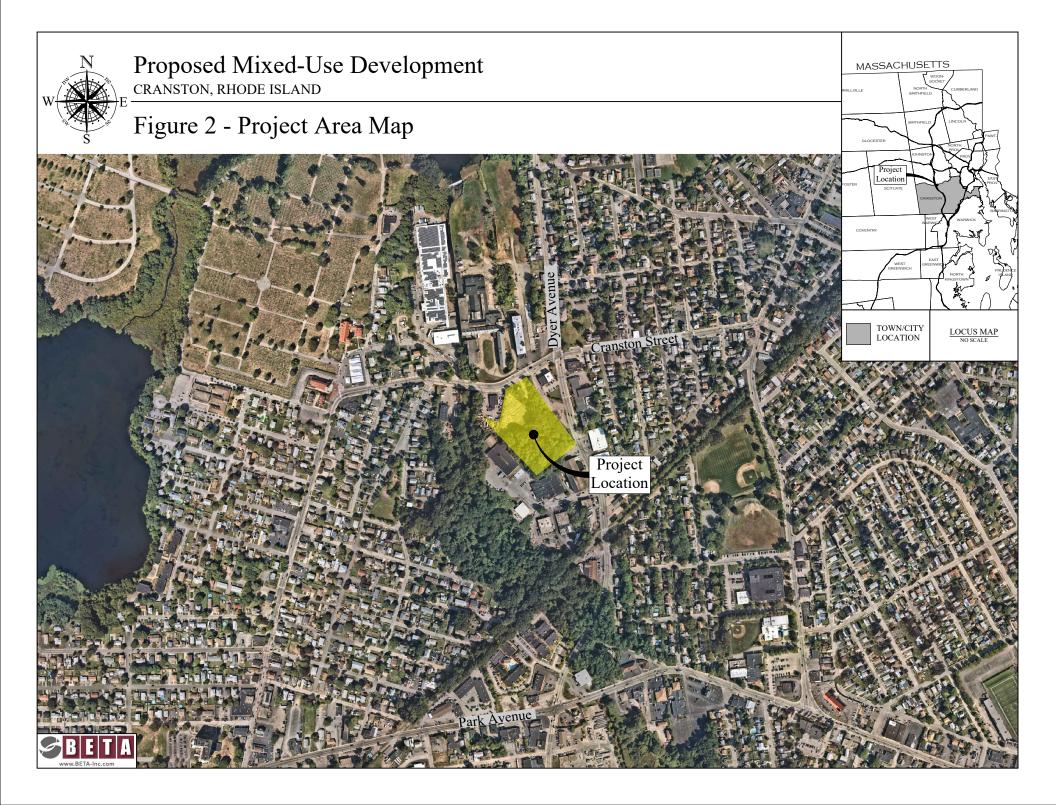
3.0 EXISTING CONDITIONS

3.1 ROADWAYS

Cranston Street

Cranston Street is classified as a major collector road throughout its entire length as it runs through the City of Cranston. Cranston Street continues northeast extending into Providence where it merges with Westminster Street. Within the project area it runs generally in an east/west direction. The roadway





provides immediate local access to abutting properties but also links to higher order facilities including,

Rhode Island State Highway Route

10 to the north.

In the project area, Cranston Street varies in typical section but adjacent to the subject property it is approximately 44-feet wide consisting of a 13-foot travel lane and a 9-foot shoulder in each direction. West of the intersection parking is restricted along the northerly side of the road and to the east parking is permitted along both sides beyond signalized the



intersection. There is no posted speed limit in the immediate project area.

Cement concrete curbing and sidewalks are available on both sides of the road. It was noted that midblock marked crosswalks are located within 150 feet to the east and west of the intersection even though there are controlled crossings at the signal. These crossing should be investigated for removal to require pedestrians to utilize the signal crossing for enhanced safety. The pavement condition can be classified as being in fair to poor condition with visible block cracking and minor rutting. Sporadic Cobra-head light fixtures on utility poles are located along the corridor for nighttime illumination of the roadway.

The Rhode Island Public Transportation Authority (RIPTA) operates a bus route along Cranston Street in the study area. Route 30 (Arlington/Oaklawn) runs seven days a week between Kennedy Plaza and CCRI in Warwick, with five major stop locations; Cranston/Webster, Cranston/Gansett, Oaklawn/Dean, Oaklawn/New London and Warwick Mall. The bus runs hourly with stops within 500 feet to the east and west of the site.

Dyer Avenue

Dyer Avenue is classified as a minor arterial roadway running in a north/south direction through the project area. Along the propety frontage, the roadway is generally 36-feet wide consisting of a 12-foot travel lane and a 6-foot shoulder in each direction, as depicted in the adjacent photograph looking north along Dyer Avenue with the subject property location on the left. The





posted speed limit for Dyer Avenue is 25 mph.

A combination of cement concrete sidewalk and asphalt sidewalk is present along both sides of the road. The pavement can be classified as being in fair condition with no visible major pavement distress, but minor cracking and crack sealing treatments as part of general roadway maintenance is visible. Sporadic cobra-head light fixtures on utility poles are located along the corridor for nighttime illumination of the roadway.

The Rhode Island Public Transportation Authority (RIPTA) operates a bus route along Dyer Avenue in the study area. Route 17 (Dyer/Pocasset) runs seven days a week between Kennedy Plaza and the Stop & Shop on Atwood Avenue in Cranston, with four major stop locations; Cranston/Westminster, Olneyville Square, Plainfield/Pocasset and Dyer/Chestnut Hill. The bus runs hourly with stops within 400 feet to the north and south of the site.

3.2 INTERSECTIONS

Cranston Street at Dyer Avenue

Dyer Avenue intersects Cranston Street to form a four-way, signalized junction. Cranston Street forms the eastern and western legs of the intersection, while Dyer Avenue makes up the northern and southern legs. Each approach to the intersection is comprised of one lane for all movements except for the southbound approach which has a separate right turn lane. The intersection was recently striped to define the approach lanes and shoulders to provide better lane control through the intersection along Cranston Street. The roadway width on the Cranston Street approaches allows for two lanes, where vehicles travelling through the junction often take advantage of the width to pass stopped, left turning traffic on

the right. This condition lends to the potential increase in angle, head-on and side-swipe crashes due to the uncertainty of vehicle movements during the permitted phases.

The traffic signal system appears to be in good operating condition. The layout of the equipment consists of mast arm mounted signal heads with in-road vehicle loop detection. It was noted that the in-road loop detector on the northbound Dyer Avenue approach was broken due to



a pot hole and was not functioning. Bracket mounted pedestrian signal heads are provided on the mast arm poles with pedestrian push buttons for enhanced pedestrian crossing control. High visibility (continental) marked crosswalk with curb ramps are provided across each approach to the intersection. It was also determined that the pushbuttons and curb ramps are not ADA compliant, missing audio



assistance for the push buttons and detectable warning panels at the curb ramps. The adjacent aerial depicts the typical characteristics of the intersection.

The intersection was determined to operate in a fully actuated mode consisting of two phases under a 70 second cycle length based upon current controller programming confirmed in the field. The first phase services all northbound and southbound movements on Dyer Avenue, while permitting concurrent pedestrian crossings along the east and west legs. As noted previously there is a broken loop detector on the northbound approach that calls Phase 1. In order to service this movement, the northbound phase is programmed to be called continuously to its maximum green time, even without a vehicle on the approach. This temporary operation caused by the lack of equipment maintenance, results in unnecessary delays on Cranston Street and less efficient operations of the overall intersection. The second phase services all eastbound and westbound movements with permitted left turns and concurrent pedestrian crossings along the north and south legs.

The fire station on Cranston Street has a mast arm with signal heads to control eastbound traffic at the driveway during pre-emption, with the main signalized junction at Dyer Avenue controlling other movements conflicting with the emergency vehicles. The stop line for the fire station is located approximately 180 feet west of the stop line for the Cranston Street eastbound approach at Dyer Avenue.

3.3 TRAFFIC DATA

Existing traffic flow characteristics for this area were developed from a traffic counting program completed by BETA Group Inc. and review of available record data from the Rhode Island Department of Transportation (RIDOT) and from a recent study completed within the project area for the adjacent *Print Works* development project located at 1381 Cranston Street. It should be noted that an advanced utility installation project on Park Avenue has been ongoing for the last several months in advance of resurfacing project to be completed by the city this summer. As part of that utility construction project, daily detours have disrupted traffic during the day creating traffic patterns along Dyer Street and Cranston Street that are not typical, or representative of average conditions. In order to be consistent with the *Print Works* development analysis, volume data from that project was compared and utilized in conjunction with the data obtained by BETA specifically for this project and record information from the RIDOT.

Specifically, BETA completed an Automated Traffic Recorder (ATR) count for a five-day period along Dyer Avenue in March 2023, while an ATR for Cranston Street was reviewed from the traffic study completed by Vanasse & Associates along with the Turning Movement Count (TMC) data for the intersection of Cranston Street with Dyer Avenue. The existing volumes obtained in January through the count program were seasonally adjusted based upon RIDOT factors for urban highways. The volumes were increased by eight percent to represent average daily traffic conditions. Complete count information can be found in the Appendix.

Based upon the seasonally adjusted turning movement count data at the intersection of Cranston Street at Dyer Avenue, Cranston Street was found to service an estimated 975 vehicles during the weekday morning peak hour between 7:30 and 8:30 AM with approximately 520 vehicles eastbound and 455 vehicles westbound. During this same period, Dyer Avenue, in the vicinity of the proposed site access



driveway, services approximately 875 vehicles with approximately 420 vehicles northbound and 455 vehicles southbound. During the weekday afternoon peak hour between 4:00 and 5:00 PM, Cranston Street was found to service 935 vehicles with approximately 430 vehicles eastbound and 505 vehicles westbound. During this same period, Dyer Avenue, in the vicinity of the proposed site access driveway, services approximately 870 vehicles with approximately 450 vehicles northbound and 420 vehicles southbound. Figure 3 on the following page depicts the daily peak hour turning movement volumes at the study intersection.

4.0 SAFETY ANALYSIS

To determine if there are any limiting factors affecting safety relating to access to the proposed mixeduse project, the physical characteristics of Dyer Avenue and Cranston Street in the project area were investigated. These limiting factors would potentially include horizontal or vertical alignment changes or roadside obstructions that limit sight distances for vehicles traveling along the road or entering the road from a side street or driveway location. In this instance, the sight distance standard is necessary to permit turning vehicles to safely enter and exit the site driveways.

The vertical and horizontal alignment of Dyer Avenue in the project area can be described as generally level and straight with slight horizontal curvature to the south, and no geometric or physical obstructions to the north through the Cranston Street intersection. Based upon the existing roadway geometry as described, the available stopping sight distances at the proposed site driveway location on Dyer Avenue are greater than 500 feet to the north and south. These values are in excess of AASHTO's recommended minimum sight distance of 155 feet based upon the posted speed limit of 25 mph and for the 250 feet based on the 85th percentile speed of 35 mph for vehicles travelling along this section of road obtained by BETA as part of the ATR data collection program.

The horizontal and vertical alignment of Cranston Street in the project area can be described as generally straight and level to the east of Dyer Avenue and curvilinear and on a decline to the west. Based upon the existing roadway geometry as described, the available stopping sight distances at the proposed site driveway locations on Cranston Street are greater than 500 feet to the east and west. These values are in excess of AASHTO's recommended minimum sight distance of 210 feet based on the 85th percentile speed of 31 miles per hour obtained from the ATR referenced in the Vanasse and Associates study as there is no posted speed limit along this section of Cranston Street.

As a result of the preliminary evaluation of the existing roadway geometry and physical features, it does not appear that any significant physical roadway safety deficiencies exist within the defined study area. Also, as part of our analysis, a review of crash statistics was completed. Data was reviewed from the City of Cranston Police Department for the latest three-year period available from January 2018 to December 2019 and from January 2022 to December 2022 that was not impacted by COVID restrictions, to determine if any location in the project area experienced a high frequency or pattern of crashes.

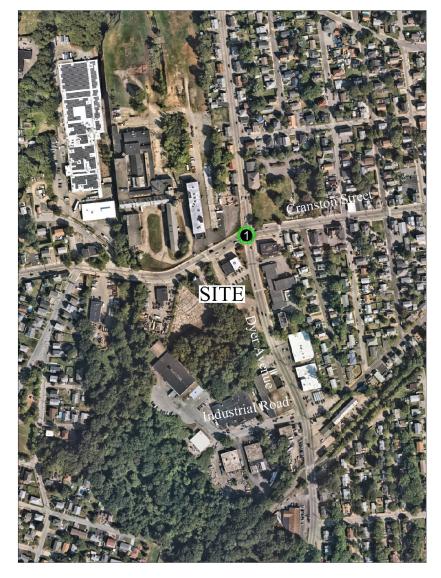
A total of 47 crashes (averaging approximately 15 per year) occurred in the project area over the threeyear study period, with none involving injuries. Summarizing the data, 37 of the crashes occurred at the

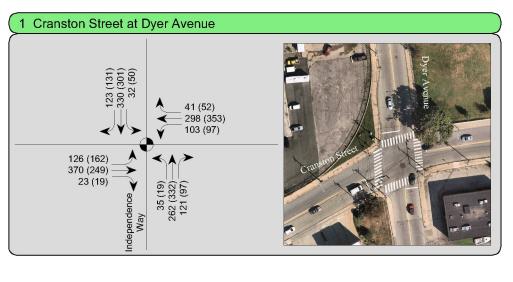


Proposed Mixed-Use Development CRANSTON, RHODE ISLAND

CRANSTON, RHODE ISLAND

Figure 3 - Existing Traffic Volumes





LEGEND:





signalized intersection of Cranston Street with Dyer Avenue, four of the crashes occurred along the segment of Cranston Street, and six of the crashes occurred along the short section of Dyer Avenue to the south of Cranston Street.

The predominant crash type at the signalized intersection of Cranston Street with Dyer Avenue was angled collisions (15), followed by rear end collisions (10), sideswipe collisions (7), head-on collisions (3), and finally single vehicle collisions (2). The majority of crashes at this location unlike most traffic signals where rear-end predominate, is the angle crash. In observing operations in the field and analyzing the crash data this type of crash can be attributed to the "permitted" control type of left turning traffic on Cranston Street, combined with the wide eastbound and westbound approaches to the intersection. The approaches, though recently striped to delineate a single lane, result in the higher crash total caused largely by drivers trying to pass on the right while a vehicle attempts to make a left turn. In these instances, left turning traffic can be blocked from seeing oncoming traffic bypassing a stopped vehicle, leading to the higher occurrence of angled collision, or misjudging the available room to pass resulting in sideswiping the vehicle queued at the stop line attempting to make a left turn.

The higher occurrence of angled collisions, though not severe resulting in only property damage, could be mitigated by restriping the intersection to actually provide separate left turn lanes that would clearly define vehicle movements through the intersection and improve sight lines for turning vehicles. Long term options that could be implemented if these types of crashes are not reduced on a yearly basis with the restriping, could be adding a phase to allow protected/permitted left turn movements on Cranston Street that would reduce vehicle conflicts and provide improved efficiency for vehicles travelling through the intersection.

The four crashes that occurred along Cranston Street included one rear end collision, one angle collision, one sideswipe collision and one single vehicle collision resulting in a low frequency of crashes and without a consistent pattern of type requiring further review. The six crashes that occurred along Dyer Avenue included one rear-end collision, three angled collisions and two single vehicle collisions. The angle collisions can all be attributed to vehicles exiting one of the many commercial driveways without having the proper gap in traffic or right of way to enter the roadway. As was the case with Cranston Street, there is an overall low occurrence of crashes (approximately two per year) that would not require additional safety improvements along the roadway.

5.0 IMPACT ANALYSIS

5.1 TRIP GENERATION

To determine the traffic impact of a proposed development, estimates of anticipated traffic to be generated by a particular land use must be calculated. As previously discussed, the development proposal consists of the construction of four, multi-family residential buildings with a total of 156 apartment units and one quality dining restaurant expected to accommodate 96 seats. The quality restaurant will have limited days of operation and would also only be open during evening hours for dinner. Access to the site will be provided via two driveways on Cranston Street and one driveway on Dyer Avenue. Figure 4 on the following page depicts the site layout and access plan provided by *DiPrete Engineering*.





Proposed Mixed-Use Development CRANSTON, RHODE ISLAND

Figure 4 - Site Layout



Site Plan provided by DiPrete Engineering



For this development, estimated traffic volumes for the mixed-use project were based on use of trip generation factors. These factors are taken from the "Trip Generation" manual, an informational report published by the Institute of Transportation Engineers (ITE), a national professional organization for traffic and transportation engineers. The data provided in the ITE report are based on extensive traffic studies for various types of land uses (residential, commercial, industrial, etc.). This data has been found to be very reliable and provides a sound basis for estimating future trips to new development projects.

For the proposed residential apartment component of the project, Land Use Code (LUC) 220 Multifamily Housing (Low-Rise) was reviewed for applicability in developing an estimate of site related vehicles trips. For the proposed quality dining restaurant, LUC 931 Fine Dining Restaurant was considered. Table 1 summarizes the peak hour site trips that have been estimated utilizing the land use code data available from the ITE manual. The appropriate worksheets from the manual are included in the Appendix, along with the trip estimate calculations. As noted, and can be seen in the table, the quality restaurant will only be open during the evening, so the weekday morning peak hour trips for this use were not calculated.

| | Description | Enter | Exit | Total |
|---|--|-----------------|----------------|----------|
| <u>Weekday AM Peak Hour</u> ITE Land Use Code 220 ITE Land Use Code 931 | Multifamily Housing (Low-Rise) Fine Dining Restaurant | 17 0 | 54 0 | 71 0 |
| | Total | <u> </u> | <u> </u> | <u> </u> |
| <u>Weekday PM Peak Hour</u> ITE Land Use Code 220 ITE Land Use Code 931 | Multifamily Housing (Low-Rise) Fine Dining Restaurant | 56 <u>17</u> | 32 <u>8</u> | 88 25 |
| | Total | 73 | 40 | 113 |

TABLE 1 – Trip Generation Estimate

5.2 FUTURE TRAFFIC CONDITIONS

In order to properly assess the impacts of a development, future traffic conditions of area roadways should be estimated for the period when the development is constructed and fully occupied. Typically, the expansion of base traffic is calculated when a project is to be constructed over an extended period (+3 to 5 years). In all instances, area growth that may affect capacity results should be considered. It is anticipated that this project would be constructed and occupied within a five-year period. Therefore, for this project, though the city has seen an annual population growth rate of less than 0.31% for the past decade, a conservative annual growth rate of 1.0 percent was utilized for the future background traffic growth to account for the average annual growth and the potential for unknown developments or redevelopments in the area.

The one percent rate was applied to the existing volumes as part of the expansion of base 2023 traffic to establish a Future 2028 No-Build condition on the servicing roadways. In addition to this base growth, coordination with the city was completed to determine the potential for site specific developments that



have been approved or will be under construction in the near future in the general area that may impact base traffic conditions. We understand there is a mixed-use development proposed at 1381 Cranston Street that will contain 129 multifamily residential apartment units and 99,920 square feet of self-storage in the existing renovated mill buildings on the property, and a total of 57,000 square feet of commercial space being allocated to cold storage in a new building. This proposed *Print Works* mixed-use development was then added to the base growth rate to establish the Future 2028 No-Build condition.

Estimated residential traffic from the *Knights Corner* mixed-use development was added to the Future 2028 No-Build condition and assigned to the local roadway network based on existing traffic patterns derived from the TMC's to establish a Future 2028 Build Condition for analysis. Traffic related to the restaurant use were primarily allocated to the proposed driveways along Cranston Street as there is intended to be an area for valet drop off at the northwest corner of the lot, with parking closest to these driveways. Figure 5 on the following page depicts the future build condition traffic demands at the study intersections analyzed in this study. Future site volume distribution figures are provided in the Appendix in the trip generation section for reference.

5.3 OPERATIONAL ANALYSIS

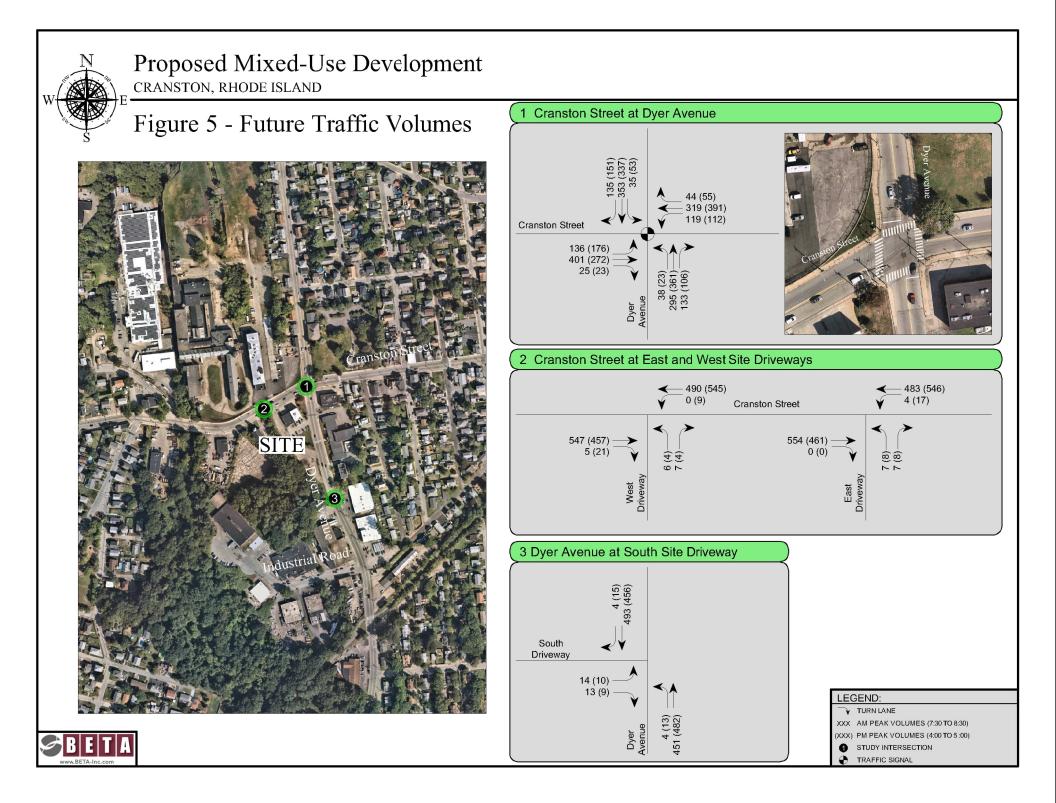
The key to any traffic impact analysis is the evaluation of roadway operations during peak traffic periods on the servicing roadway system. This situation would occur when the site-generated traffic, combined with the traffic volumes on the main roadway, result in the highest one-hour volume serviced along a roadway segment, or through an intersection. Review of record traffic data found that the weekday morning and afternoon peak hours would represent this worst-case combination of site-generated traffic with the servicing roadway peak traffic period.

The Highway Capacity Manual methodology provides the most accurate means of evaluating traffic capacity and delays for roadways and intersections. The results of these procedures are expressed in terms of Level of Service (LOS). Level of Service is a qualitative measure of traffic flow efficiency based on anticipated vehicle delays. For example, LOS "A" represents the best condition with little or no delay, while LOS "F" indicates that the roadway/intersection is beyond capacity resulting in extended vehicle delays and potential queuing. Table 2 outlines the Level of Service delay criteria presented in the Highway Capacity Manual for signalized and unsignalized intersections.

| Unsignalized Delay Per Vehicle (sec) | Signalized Delay Per Vehicle (sec) |
|---|--|
| <10 | <10 |
| >10 and <15 | >10 and <20 |
| >15 and <25 | >20 and <35 |
| >25 and <35 | >35 and <55 |
| >35 and <50 | >55 and <80 |
| >50 | >80 |
| | Per Vehicle (sec) <10 >10 and <15 >15 and <25 >25 and <35 >35 and <50 |

TABLE 2 – Highway Capacity Manual Criteria





The existing signalized intersection of Cranston Street at Dyer Avenue as well as the proposed unsignalized site driveway intersections along Cranston Street and Dyer Avenue were analyzed. The capacity analysis worksheets are included in the Appendix and Tables 3 through 5 summarizes the results of the analyses.

Table 3 depicts the operations of the traffic signal under existing traffic demand conditions analyzed utilizing existing timing data obtained from the controller. As noted previously there is a defective loop detector on the Dyer Avenue northbound approach that requires a *recall* setting in order to be serviced. This *recall* is set to its maximum available green time of 25 seconds which runs regardless of the approach demand, resulting in lost time and inefficient operations of the traffic signal to the detriment of the Cranston Street eastbound/westbound movements. These delays were documented in the *Print Works* study completed by Vanasse & Associates, Inc., but for this analysis, the intersection was assumed to be operating properly as designed with actuated loop detection once the detector is replaced. This will provide a better understanding of expected conditions at the junction.

| | EXISTING CONDITIONS | | | | | | | | |
|-------------------------------|------------------------------------|-------|--------------------|------|-----|-------|--------------------|------|--|
| | | AM | Peak Hour | | | PM | Peak Hour | | |
| Location / Movement | | | 95 th % | | | | 95 th % | | |
| | LOS | Delay | Queue | v/c | LOS | Delay | Queue | v/c | |
| | | | Length (veh.) | | | | Length (veh.) | | |
| Cranston Street at Dyer Avenu | Cranston Street at Dyer Avenue (S) | | | | | | | | |
| Cranston Street EB All | С | 29.7 | 16 | 0.86 | С | 26.5 | 13 | 0.81 | |
| Cranston Street WB All | С | 21.2 | 11 | 0.74 | В | 18.6 | 11 | 0.72 | |
| Dyer Avenue NB All | С | 32.5 | 13 | 0.83 | С | 25.9 | 11 | 0.76 | |
| Dyer Avenue SB Left/Thru | С | 24.8 | 9 | 0.68 | С | 23.5 | 9 | 0.66 | |
| Dyer Avenue SB Right | А | 6.3 | 2 | 0.23 | А | 5.3 | 2 | 0.22 | |
| OVERALL | С | 25.8 | - | - | С | 22.2 | - | - | |

(S) – Signalized

As can be seen in the table, the signalized intersection was determined to operate overall at LOS C during both the AM and PM peak periods, which presently operate under the same cycle length and split times. There is no Time of Day (TOD) plan programmed into the controller to account for varying traffic demand conditions during these different peak periods. All critical movements operate in an acceptable manner during the morning and afternoon peak hours with the northbound and eastbound approaches experiencing the greatest delays operating with average delays of less than 35 seconds at LOS C.

Table 4 presents the future design period taking into consideration only base traffic growth, as well as known developments including the proposed *Print Works* project at 1381 Cranston Street recently approved by the city. The subject development is not included in this "No-Build" analysis scenario. The

analysis utilized existing timings as they represent optimized splits for the volumes serviced during the daily peak hours.

As can be seen in the table, the signalized intersection of Cranston Street at Dyer Avenue continues to operate overall at LOS C during the morning and afternoon peak hours, similar to existing conditions. The critical northbound and eastbound movements continue to operate in an acceptable manner at LOS D or better during the daily peak traffic conditions.

| | FUTURE 2028 NO BUILD CONDITIONS | | | | | | | |
|-------------------------------|---------------------------------|-------|--------------------|------|-----|-------|--------------------|------|
| | | AM | Peak Hour | | | PM | Peak Hour | |
| Location / Movement | | | 95 th % | | | | 95 th % | |
| | LOS | Delay | Queue | v/c | LOS | Delay | Queue | v/c |
| | | | Length (veh.) | | | | Length (veh.) | |
| Cranston Street at Dyer Avenu | ie (S) | | | | | | | |
| Cranston Street EB All | D | 39.8 | 17 | 0.93 | С | 32.1 | 14 | 0.86 |
| Cranston Street WB All | С | 28.3 | 14 | 0.83 | С | 21.1 | 12 | 0.76 |
| Dyer Avenue NB All | D | 44.7 | 15 | 0.92 | С | 30.2 | 14 | 0.81 |
| Dyer Avenue SB Left/Thru | С | 26.6 | 11 | 0.71 | С | 27.5 | 10 | 0.73 |
| Dyer Avenue SB Right | А | 6.6 | 2 | 0.24 | А | 5.9 | 2 | 0.24 |
| OVERALL | С | 33.4 | - | - | С | 25.9 | - | - |

TABLE 4 – Level of Service Summary (Future No-Build Conditions)

(S) – Signalized

Table 5 on the following page presents the future traffic demand conditions when the project is anticipated to be constructed and fully occupied. The analysis during this period includes the main study signalized intersection of Cranston Street at Dyer Avenue, as well as the proposed site driveway intersections. During the future build period, it is anticipated that the signalized intersection of Cranston Street at Dyer Avenue that the signalized intersection of Cranston Street at Dyer Avenue will operate at an acceptable LOS D during the morning peak hour and LOS C during the afternoon peak hour. The critical northbound and eastbound movements continue to operate in an acceptable manner at LOS D or better during the daily peak traffic conditions.

In addition to the main signalized junction the proposed unsignalized site driveway intersections were also evaluated to demonstrate they will operate in an acceptable manner without excessive delays or traffic congestion. As seen in the table both Cranston Street driveways will operate efficiently with all critical movements operating at LOS C or better, with typically only one car expected to be queued on the site driveway waiting to enter the Cranston Street traffic stream. Similarly, the Dyer Avenue driveway will operate with minor acceptable delays of under 20 seconds and typically only one vehicle waiting to turn out of the driveway to enter Dyer Avenue and negligible delays for left turn site entering traffic.



| | FUTURE 2028 BUILD CONDITIONS | | | | | | | | |
|---------------------------------|--------------------------------------|-------|--------------------|------|--------------|-------|--------------------|------|--|
| | | AM | Peak Hour | | PM Peak Hour | | | | |
| Location / Movement | | | 95 th % | | | | 95 th % | | |
| | LOS | Delay | Queue | v/c | LOS | Delay | Queue | v/c | |
| | | | Length (veh.) | | | | Length (veh.) | | |
| Cranston Street at Dyer Avenu | e (S) | | | | | | | | |
| Cranston Street EB All | D | 44.4 | 18 | 0.95 | D | 35.4 | 15 | 0.88 | |
| Cranston Street WB All | С | 30.7 | 14 | 0.86 | С | 22.4 | 14 | 0.78 | |
| Dyer Avenue NB All | D | 51.8 | 16 | 0.95 | С | 32.2 | 14 | 0.83 | |
| Dyer Avenue SB Left/Thru | С | 26.9 | 11 | 0.71 | С | 29.5 | 12 | 0.76 | |
| Dyer Avenue SB Right | Α | 6.5 | 2 | 0.24 | Α | 6.1 | 2 | 0.25 | |
| OVERALL | D | 37.0 | - | - | С | 27.9 | - | - | |
| Cranston Street at Eastern Driv | /eway | (U) | | | | | | | |
| Cranston Street WB Left | А | 8.7 | 0 | 0.01 | А | 8.4 | 0 | 0.02 | |
| Site Driveway NB All | С | 17.3 | 1 | 0.05 | С | 17.1 | 1 | 0.06 | |
| Cranston Street at Western Dr | iveway | (U) | | | | | | | |
| Cranston Street WB Left | А | 0.0 | 0 | 0.00 | А | 8.5 | 0 | 0.01 | |
| Site Driveway NB All | С | 16.8 | 1 | 0.04 | С | 16.5 | 1 | 0.03 | |
| Dyer Avenue at Southern Drive | Dyer Avenue at Southern Driveway (U) | | | | | | | | |
| Site Driveway EB All | С | 16.5 | 1 | 0.09 | С | 16.5 | 1 | 0.06 | |
| Dyer Avenue NB Left | А | 8.5 | 1 | 0.01 | А | 8.5 | 0 | 0.01 | |

| TABLE 5 – Level of Service Summary | (Future Build Conditions) |
|------------------------------------|---------------------------|
|------------------------------------|---------------------------|

(S) – Signalized

(U) - Unsignalized

Though as indicated in Table 5 that acceptable intersection operations will be maintained under the future build condition we also, as part of this study, completed an additional analysis to address the observed operations of the signalized intersection that result in unnecessary delays and increased potential for crashes. Specifically, as noted earlier in the report, the wide 44 foot Cranston Street approaches permit thru traffic to pass stopped left turning traffic at the intersection. This condition is random based upon driver behavior and aggressiveness resulting in unpredictable, last minute driver decisions when traversing the intersection. The single approach lane also results in a less efficient operation as thru traffic is regularly delayed for stopped left turning traffic on their approach.

An alternative to better control eastbound and westbound movements through the intersection would be to formalize separate left turn lanes on these approaches. In doing so, thru and left turning movements will be clearly defined for the drivers, providing a better understanding of conditions to make proper decisions of whether to yield or turn in the available gaps, theoretically improving intersection safety. This design would also improve intersection inefficiencies as discussed previously, by reducing the potential of left turning traffic hindering thru traffic flow, therefore reducing overall delays and queuing on the approaches.



The analysis has been provided in the Appendix for reference where it is demonstrated that delays are greatly reduced, improving operations during both the morning and afternoon peaks where overall they would operate at an LOS B. The critical northbound and eastbound movements would also operate at LOS C or better, improving operations over all periods analyzed as part of this study. Also, as previously noted, if angle crashes are not reduced as would be anticipated with the restriping for exclusive left turn lanes, an additional measure could be implemented long term to provide an advanced protected control of the left turning traffic on Cranston Street. This protected/permitted control of the left turning conflicts that occur with only the permitted control, and the intersection would also continue to operate in an acceptable manner with reduced delays and enhanced safety.

6.0 Conclusions and Recommendations

In summary, the study has shown that the proposed mixed-use development project access and circulation plan has been designed to provide a level of traffic safety and efficiency on the servicing roadway system. The proposed site driveway intersections were determined to provide sufficient sight distances in accordance with AASHTO criteria for visibility and decision making of drivers attempting to enter/exit main street traffic from the proposed site driveways.

The results of the operational analysis determined that the estimated increase in traffic during the peak periods resulting from the proposed *Knights Corner* development project will have a minor impact on overall traffic operations along Cranston Street and Dyer Avenue and specifically at their signalized junction.

In reference to safety and operations it is recommended, as discussed earlier in the study, the following measures could be implemented at the signalized intersection of Cranston Street with Dyer Avenue as part of a general signal maintenance and optimization program:

- 1. Restripe the Cranston Street intersection approaches to provide exclusive left turn lanes.
- 2. Remove mid-block crosswalks on Cranston Street that are in close proximity to the controlled signalized pedestrian crossings at the Cranston Street/Dyer Avenue intersection.
- 3. Replace the existing malfunctioning loop detector on the northbound Dyer Avenue approach.

Therefore, based upon the data collected on the servicing roadways, the analysis completed as part of this study, along with the access design and other recommendations identified, the proposed mixed-use project was determined to have adequate and safe access to a public street, and will not have an adverse impact on public safety and welfare in the study area.

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ⁱAerial Images provided in this document were obtained from Nearmap.

APPENDIX

- A. Traffic Volume Data
- B. Traffic Crash Data
- C. Trip Generation
- D. Operational Analysis



APPENDIX A – Traffic Volume Data

Automatic Traffic Recorder Count

Cranston Street

Dyer Avenue

Intersection Turning Movement Count

Cranston Street at Dyer Avenue



A

Automatic Traffic Recorder Count

Cranston Street Dyer Avenue



Cranston Street

(Source; Vanasse and Associates, January 2023)

(Source; RIDOT 1994 - 2019)



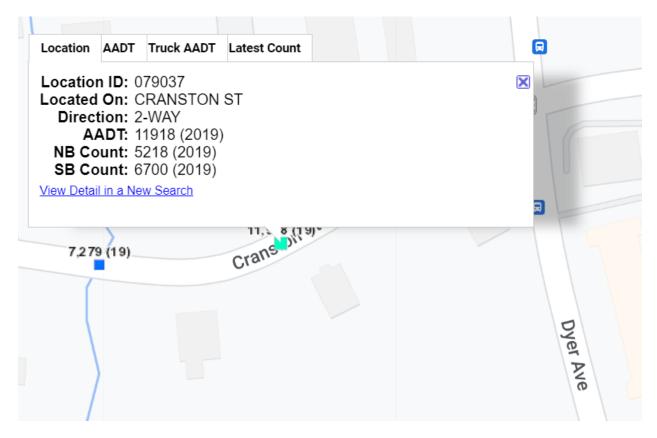
Traffic Volumes



CRANSTON ST. Cranston- STATION 079037

| AADT | 0 | | | | | | |
|------|------|--------|--------|-----|-----|--------------|----------|
| | Year | AADT | DHV-30 | K % | D % | PA | BC |
| | 2019 | 11,918 | | | | 11,195 (94%) | 722 (6%) |

LOCATION OF STATION 079037:



HISTORICAL DATA FROM STATION 070032 (IN SAME AREA AS STATION 079037):

| | 00PHIL | | | | | | | | | | |
|------|----------------|------------------------------|------------|-------|------|--------|--------|-------|------|--|--|
| Town | Roadway | Segment | StationNo | AADT | Date | Bridge | PeakHr | Funcl | Loop | | |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 0700320170 | 15300 | 1994 | 099501 | 7 | 16 | S | | |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 0700320170 | 16500 | 1996 | 099501 | 7 | 16 | S | | |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 0700320170 | 13700 | 2000 | 099501 | 7 | 16 | S | | |

| | | 00 | PHIL | | | | | | |
|------|----------------|------------------------------|-----------|-------|------|--------|--------|-------|------|
| Town | Roadway | Segment | StationNo | AADT | Date | Bridge | PeakHr | Funcl | Loop |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 12300 | 2004 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 13200 | 2006 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 14700 | 2007 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 14100 | 2013 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 12600 | 1995 | 099501 | 7 | 16 | S |
| | | 00 | PHIL | | | | | | |
| Town | Roadway | Segment | StationNo | AADT | Date | Bridge | PeakHr | Funcl | Loop |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 13600 | 1999 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 14000 | 2012 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 11000 | 2008 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 11800 | 1988 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 13300 | 1991 | 099501 | 7 | 16 | S |
| 07 | CRANSTON ST | BTW MATHEWSON & VALONE RD | 070032 | 12700 | 1993 | 099501 | 7 | 16 | S |

Transportation Data Corporation Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999

Cranston Street west of Dyer Avenue City, State: Cranston, RI Client: VAI/D. Roach

| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | Start | 10-Jan-23 EB | | Hour | Totals | WE | 3 | Hour | Totals | Combined Totals | | |
|---|-------------------|--------------|------|----------|--------|-----|------|------|--------|-----------------|------|------|
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | fternoon | | | | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | 95 | | | 9 | 140 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 12:15 | | | | | | 8 | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 12:30 | | 4 | 83 | | | 2 | 113 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | 0 | | 17 | 366 | 2 | 123 | 21 | 494 | 38 | 860 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 01:00 | | 2 | 79 | | | 2 | 121 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | 2 | | | | 7 | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 01:30 | | 7 | 83 | | | 6 | 113 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | 5 | | 16 | 327 | | 122 | 16 | 472 | 32 | 799 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 02:00 | | 2 | | | | 5 | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | | | | 5 | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 02:30 | | 1 | 105 | | | 3 | 120 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | | 5 | 385 | | | 16 | 445 | 21 | 830 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 03:00 | | 6 | 102 | | | 6 | 100 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | 0 | | | | 3 | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 03:30 | | 5 | | | | 3 | 107 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | 6 | | 17 | 417 | | | 12 | 408 | 29 | 825 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 04:00 | | 2 | | | | 0 | 114 | | | | |
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| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 04:30 | | | 88 | | | 2 | | | | | |
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| 05:30 24 74 72 295 17 69 45 377 117 67 06:00 27 63 16 75 16 75 117 66 37 67 67 66 37 67 67 66 37 67 67 66 37 67 67 66 37 77 78 78 36 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 77 78 78 78 78 78 78 78 78 79 78 76 74 34 <td>05:00</td> <td></td> <td>8</td> <td></td> <td></td> <td></td> <td>5</td> <td></td> <td></td> <td></td> <td></td> <td></td> | 05:00 | | 8 | | | | 5 | | | | | |
| 05:45 26 72 72 295 17 69 45 377 117 67 06:00 27 63 16 75 29 75 | | | | | | | | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | 24 | 74 | | | 15 | 86 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | | 72 | 295 | | | 45 | 377 | 117 | 672 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 06:00 | | 27 | 63 | | | 16 | 75 | | | | |
| 06:45 71 60 199 241 54 55 152 261 351 50 07:00 77 46 66 37 66 37 76 77 77 66 77 <td></td> <td></td> <td></td> <td>59</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | | 59 | | | | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 06:30 | | 55 | 59 | | | 53 | 56 | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | 71 | 60 | 199 | 241 | | 55 | 152 | 261 | 351 | 502 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 07:00 | | 77 | 46 | | | 66 | 37 | | | | |
| 07:45 114 36 401 161 118 27 357 179 758 34 08:00 132 21 97 35 97 35 179 758 34 08:00 132 20 88 49 97 35 179 758 34 08:15 102 20 88 49 97 35 179 758 34 08:45 86 38 430 110 98 33 378 145 808 25 09:00 88 24 82 27 16 17 160 16 311 93 91 20 336 107 647 20 20 100 10< | | | | | | | | | | | | |
| 08:00 132 21 97 35 102 10 | 07:30 | | 109 | 36 | | | 85 | 51 | | | | |
| 08:15 102 20 88 49 | | | 114 | | 401 | 161 | | | 357 | 179 | 758 | 340 |
| 08:30 110 31 95 28 08:45 86 38 430 110 98 33 378 145 808 25 09:00 88 24 82 27 76 145 808 25 09:15 80 26 89 26 6 6 100 100 647 20 09:30 74 27 74 34 7 74 34 7 74 34 7 74 100 647 20 100 647 20 100 647 20 100 100 647 20 100 100 647 20 100 | 08:00 | | 132 | 21 | | | 97 | 35 | | | | |
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| 09:00 88 24 82 27 09:15 80 26 89 26 09:30 74 27 74 34 09:45 69 16 311 93 91 20 336 107 647 20 10:00 63 34 91 17 74 34 74 74 20 10:00 63 34 91 17 76 647 20 76 10 | 08:30 | | 110 | 31 | | | 95 | 28 | | | | |
| 09:15 80 26 89 26 09:30 74 27 74 34 09:45 69 16 311 93 91 20 336 107 647 20 10:00 63 34 91 17 17 17 17 1015 67 20 89 11 103 19 19 17 1015 67 20 103 19 101 | | | | 38 | 430 | 110 | 98 | 33 | 378 | 145 | 808 | 25 |
| 09:30 74 27 74 34 09:45 69 16 311 93 91 20 336 107 647 20 10:00 63 34 91 17 74 107 647 20 10:15 67 20 89 11 74 | | | 88 | 24 | | | | 27 | | | | |
| 09:45 69 16 311 93 91 20 336 107 647 20 10:00 63 34 91 17 17 17 101 | | | 80 | | | | 89 | | | | | |
| 10:00 63 34 91 17 10:15 67 20 89 11 10:30 68 12 103 19 10:45 75 12 273 78 96 13 379 60 652 13 11:00 74 12 110 15 111 15 111 15 111 15 111 15 111 15 111 15 111 15 111 15 111 15 111 111 15 111 | 09:30 | | 74 | 27 | | | | 34 | | | | |
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| 10:30 68 12 103 19 10:45 75 12 273 78 96 13 379 60 652 13 11:00 74 12 110 15 110 15 1111 1111 1111 <td>10:00</td> <td></td> <td>63</td> <td>34</td> <td></td> <td></td> <td>91</td> <td>17</td> <td></td> <td></td> <td></td> <td></td> | 10:00 | | 63 | 34 | | | 91 | 17 | | | | |
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| 11:15 63 9 102 16 11:30 70 9 148 13 11:45 80 9 287 39 97 8 457 52 744 9 Total 2053 2889 2178 3432 4231 632 Combined 4942 5610 10552 | | | 75 | | 273 | 78 | | | 379 | 60 | 652 | 138 |
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| Total 2053 2889 2178 3432 4231 632 Combined 4942 5610 10552 Total | | | 70 | 9 | | | 148 | 13 | | | | |
| Combined 4942 5610 10552 | 11:45 | | | | 287 | 39 | 97 | | 457 | 52 | 744 | 91 |
| Total 4942 5610 10552 | Total | | 2053 | 2889 | | | 2178 | 3432 | | | 4231 | 6321 |
| created | Combined Total | | 4942 | | | | 5610 | 0 | | | 1055 | 52 |
| | Percentag | 0.0% | | | | | | | | | | |

ag e

0.0%

05662Avolume Site Code: 9575

Transportation Data Corporation Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999

Cranston Street west of Dyer Avenue City, State: Cranston, RI Client: VAI/D. Roach

| Start | 11-Jan-23 | EB | | Hour | Totals | WB | | Hour | Totals | Combined | Totals |
|----------------|-----------|-----------|-----------|---------|-----------|-------------|-----------|------|-----------|----------|--------|
| Time | Wed | Morning A | Afternoon | Morning | Afternoon | Morning A | Afternoon | | Afternoon | Morning | |
| 12:00 | | õ | 86 | - | | 11 | 138 | - | | - | |
| 12:15 | | 4 | 77 | | | 6 | 125 | | | | |
| 12:30 | | 1 | 80 | | | 4 | 115 | | | | |
| 12:45 | | 1 | 97 | 12 | 340 | 3 | 119 | 24 | 497 | 36 | 837 |
| 01:00 | | 3 | 90 | | | 3 | 127 | | | | |
| 01:15 | | 4 | 72 | | | 7 | 106 | | | | |
| 01:30 | | 2 | 80 | | | 4 | 135 | | | | |
| 01:45 | | 4 | 90 | 13 | 332 | 3 | 110 | 17 | 478 | 30 | 810 |
| 02:00 | | 1 | 92 | | 002 | 2 | 126 | | | 00 | 0.0 |
| 02:15 | | 1 | 101 | | | 3 2 5 | 116 | | | | |
| 02:30 | | | 120 | | | 4 | 80 | | | | |
| 02:45 | | 0 3 | 102 | 5 | 415 | 2 | 122 | 13 | 444 | 18 | 859 |
| 02:40 | | 0 | 102 | 5 | 415 | 2 | 110 | 15 | | 10 | 008 |
| | | 0 2 | 102 | | | 1 | | | | | |
| 03:15 | | 2 | 100 | | | | 105 | | | | |
| 03:30 | | 3 | 130 | 0 | 400 | 0 | 123 | 0 | 100 | 10 | 0.00 |
| 03:45 | | 4 | 106 | 9 | 438 | 6 | 84 | 9 | 422 | 18 | 860 |
| 04:00 | | 4 | 104 | | | 4 | 96 | | | | |
| 04:15 | | 4 | 104 | | | 3 | 117 | | | | |
| 04:30 | | 9 | 113 | | | 2 5 | 113 | | | | |
| 04:45 | | 12 | 76 | 29 | 397 | | 113 | 14 | 439 | 43 | 836 |
| 05:00 | | 8 17 | 96 | | | 4 | 91 | | | | |
| 05:15 | | 17 | 70 | | | 13 | 112 | | | | |
| 05:30 | | 18 | 75 | | | 12 | 90 | | | | |
| 05:45 | | 35 | 66 | 78 | 307 | 17 | 73 | 46 | 366 | 124 | 673 |
| 06:00 | | 26 | 73 | | | 12 | 67 | | | | |
| 06:15 | | 44 | 63 | | | 30 | 62 | | | | |
| 06:30 | | 52 | 56 | | | 39 | 55 | | | | |
| 06:45 | | 70 | 38 | 192 | 230 | 62 | 67 | 143 | 251 | 335 | 481 |
| 07:00 | | 95 | 62 | 192 | 250 | 60 | 48 | 145 | 201 | 555 | 401 |
| 07:15 | | 87 | 40 | | | 87 | 58 | | | | |
| | | | | | | | | | | | |
| 07:30 | | 123 | 39 | 400 | 470 | 82 | 50 | 200 | 045 | 704 | 004 |
| 07:45 | | 133 | 35 | 438 | 176 | 94 | 59 | 323 | 215 | 761 | 391 |
| 08:00 | | 126 | 32 | | | 95 | 48 | | | | |
| 08:15 | | 89 | 31 | | | 74 | 44 | | | | |
| 08:30 | | 96 | 37 | | | 91 | 37 | | | | |
| 08:45 | | 89 | 40 | 400 | 140 | 121 | 44 | 381 | 173 | 781 | 313 |
| 09:00 | | 97 | 38 | | | 78 | 32 | | | | |
| 09:15 | | 81 | 34 | | | 86 | 30 | | | | |
| 09:30 | | 59 | 20 | | | 98 | 20 | | | | |
| 09:45 | | 93 | 27 | 330 | 119 | 93 | 35 | 355 | 117 | 685 | 236 |
| 10:00 | | 71 | 22 | | | 94 | 26 | | | | |
| 10:15 | | 85 | 13 | | | 83 | 26 | | | | |
| 10:30 | | 77 | 15 | | | 80 | 12 | | | | |
| 10:45 | | 73 | 11 | 306 | 61 | 96 | 14 | 353 | 78 | 659 | 139 |
| 11:00 | | 76 | 11 | 000 | 01 | 94 | 8 | 000 | , 0 | 000 | 100 |
| 11:15 | | 66 | 11 | | | 100 | 18 | | | | |
| 11:30 | | 87 | 3 | | | 100 | 7 | | | | |
| 11:45 | | 96 | 13 | 325 | 38 | 122 | 13 | 439 | 46 | 764 | 0. |
| | | | | 320 | 30 | | | 439 | 40 | | 84 |
| Total | | 2137 | 2993 | | | 2117 | 3526 | | | 4254 | 6519 |
| Combined | | 5130 | | | | 5643 | 3 | | | 1077 | 3 |
| Total | | 2.00 | | | | | | | | | |
| Percentag e | 0.0% | | | | | | | | | | |
| Total | | 4190 | 5882 | | | 4295 | 6958 | | | 8485 | 12840 |
| Percent | | 41.6% | 58.4% | | | 38.2% | 61.8% | | | 39.8% | 60.2% |
| | | | | | | | | | | | / (|

Page 2

05662Avolume Site Code: 9575

Speeds



Transportation Data Corporation

Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999

Cranston Street

west of Dyer Avenue

City, State: Cranston, RI

05662Aspeed

Site Code: 9575

Client: VAI/D. Roach Eastbound Start 85th 95th Time Total Percent Percent 01/10/23 01:00 02:00 03:00 04:00 05:00 06:00 07:00 08:00 09:00 10:00 11:00 12 PM 13:00 14:00 15:00 16:00 17:00 18:00 19:00 20:00 21:00 22:00 23:00 Total Percent 19.2% 17.1% 37.2% 23.1% 3.2% 0.2% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 08:00 AM Peak 07:00 08:00 09:00 08:00 05:00 09:00 11:00 08:00 Vol PM Peak 15:00 18:00 15:00 15:00 16:00 15:00 14:00 14:00 Vol.

Page 1

Transportation Data Corporation

Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999 05662Aspeed

95th

Percent

west of Dyer Avenue City, State: Cranston, RI Client: VAI/D. Roach Eastbound Start Time 01/11/23 01:00 02:00 03:00 04:00 05:00 06:00 07:00 08:00 09:00 10:00 11:00 12 PM 13:00 14:00 15:00 16:00 17:00 18:00 19:00 20:00 21:00 22:00 23:00 Total Percent 19.9% 18.3% 37.1% 21.4% 2.9% 0.3% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 11:00 AM Peak 07:00 07:00 10:00 09:00 05:00 08:00 10:00 Vol 22:00 14:00 17:00 PM Peak 16:00 14:00 15:00 13:00 12:00 19:00 Vol. Grand Total 37.2% 3.0% 0.2% 19.6% 17.7% 22.2% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Percent 15th Percentile : 11 MPH 50th Percentile : 21 MPH 27 MPH 85th Percentile : 95th Percentile : 29 MPH Stats 10 MPH Pace Speed : 21-30 MPH Number of Vehicles > 30 MPH :

Cranston Street

Percent of Vehicles > 30 MPH :

Mean Speed(Average) :

3.3% 21 MPH Page 2

Site Code: 9575

85th

Percent

Total

07:00

15:00

Transportation Data Corporation Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999

Cranston Street

05662Aspeed Site Code: 9575

| west of Dy City, State | yer Avenu : Cranstoi | n, RI | | | | Site Code: 9575 | | | | | | | | | | | |
|---------------------------|-------------------------|----------|----------------|----------|----------|-----------------|----------|----------|------------|----------|----------|----------------|----------|-------|-----------------|---------------|--|
| Client: VA | $\Lambda I/D$. R0a | acn | | | | | | | | | | | | | | | |
| Westbound | 1 | 10 | 24 | | 01 | 20 | 44 | 40 | F 4 | 50 | <u> </u> | | 74 | | 0546 | 0546 | |
| Start | 15 | 16 20 | 21 | 26 | 31 35 | 36 | 41 45 | 46 50 | 51 55 | 56 60 | 61 65 | 66 70 | 71 75 | Total | 85th Percent | 95th | |
| | 0 | 20 | <u>25</u> 3 | <u> </u> | <u> </u> | <u>40</u> 0 | <u> </u> | 0 | <u></u> 0 | 0 | 0 | <u>70</u> 0 | 0 | 21 | <u>32</u> | Percent 34 | |
| 01:00 | 1 | 0 | 3 | 6 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 33 | 35 | |
| 02:00 | 0 | 1 | 2 | 7 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 34 | 37 | |
| 03:00 | 0 | 0 | 6 | 5 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 29 | 31 | |
| 04:00 | 0 | 0 | 0 | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 33 | 34 | |
| 05:00 | 1 | 0 | 8 | 27 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 31 | 34 | |
| 06:00 | 4 | 3 | 32 | 81 | 30 | 1 | 1 | Õ | Õ | Õ | Ő | 0 | Õ | 152 | 31 | 34 | |
| 07:00 | 12 | 2 | 78 | 183 | 72 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 357 | 31 | 34 | |
| 08:00 | 17 | 7 | 79 | 201 | 70 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 378 | 31 | 33 | |
| 09:00 | 16 | 3 | 84 | 167 | 60 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 336 | 31 | 34 | |
| 10:00 | 8 | 12 | 79 | 217 | 61 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 379 | 30 | 33 | |
| 11:00 | 44 | 26 | 109 | 203 | 70 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 457 | 30 | 33 | |
| 12 PM | 14 | 5 | 100 | 276 | 91 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 494 | 31 | 34 | |
| 13:00 | 19 | 7 | 104 | 257 | 81 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 472 | 30 | 33 | |
| 14:00 | 24 | 4 | 76 | 247 | 82 | 11 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 445 | 31 | 34 | |
| 15:00 | 19 | 7 | 67 | 231 | 77 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 408 | 31 | 34 | |
| 16:00 | 18 | 5 | 88 | 239 | 79 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 432 | 31 | 33 | |
| 17:00 | 12 | 2 | 78 | 219 | 61 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 377 | 30 | 33 | |
| 18:00 | 7 | 4 | 40 | 155 | 53 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 261 | 31 | 33 | |
| 19:00 | 5 | 0 | 36 | 97 | 36 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 179 | 31 | 34 | |
| 20:00 | 0 | 2 | 21 | 87 | 32 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 145 | 32 | 34 | |
| 21:00 | 2 | 1 | 22 | 58 | 22 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 107 | 31 | 34 | |
| 22:00 | 0 | 0 | 3 | 39 | 17 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 60 | 32 | 34 | |
| 23:00 | 0 | 0 | 8 | 37 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 52 | 29 | 33 | |
| Total | 223 | 91 | 1126 | 3055 | 1029 | 79 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 5610 | | | |
| Percent | 4.0% | 1.6% | 20.1% | 54.5% | 18.3% | 1.4% | 0.1% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | | | | |
| AM Peak | 11:00 | 11:00 | 11:00 | 10:00 | 07:00 | 07:00 | 06:00 | | | | | | | 11:00 | | | |
| Vol. | 44 | 26 | 109 | 217 | 72 | 9 | 10.00 | 22.00 | | | | | | 457 | | | |
| PM Peak | 14:00 | 13:00 | 13:00 | 12:00 | 12:00 | 14:00 | 12:00 | 22:00 | | | | | | 12:00 | | | |
| Vol. | 24 | 7 | 104 | 276 | 91 | 11 | 1 | 1 | | | | | | 494 | | | |

Transportation Data Corporation Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999

05662Aspeed Site Code: 9575

Page 4

Cranston Street west of Dyer Avenue City, State: Cranston, RI Client: VAI/D. Roach Westbound

| Westbound | | | | | | | | | | | | | | | | |
|--------------------|--------------------|----------|--------------------------|--------------|-----------------------|----------------------|-------|----------|----------|------|------|------|------|-------|---------|---------|
| Start | 1 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | | 85th | 95th |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | Total | Percent | Percent |
| 01/11/23 | 0 | 0 | 4 | 14 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 32 | 34 |
| 01:00 | 0 | 0 | 3 | 4 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 36 | 38 |
| 02:00 | 0 | 0 | 3 | 5 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 33 | 36 |
| 03:00 | 0 | 1 | 1 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 33 | 34 |
| 04:00 | 0 | 0 | 3 | 8 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 32 | 36 |
| 05:00 | 1 | 0 | 8 | 29 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 46 | 30 | 33 |
| 06:00 | 3 | 1 | 39 | 71 | 27 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 143 | 31 | 34 |
| 07:00 | 14 | 3 | 64 | 177 | 60 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 323 | 31 | 34 |
| 08:00 | 23 | 5 | 79 | 192 | 71 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 381 | 31 | 34 |
| 09:00 | 6 | 3 | 85 | 197 | 58 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 355 | 30 | 33 |
| 10:00 | 11 | 7 | 90 | 174 | 64 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 353 | 31 | 34 |
| 11:00 | 15 | 4 | 63 | 260 | 94 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 439 | 31 | 33 |
| 12 PM | 14 | 3 | 102 | 270 | 102 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 497 | 31 | 34 |
| 13:00 | 15 | 7 | 106 | 253 | 91 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 478 | 31 | 34 |
| 14:00 | 21 | 2 | 106 | 232 | 74 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 444 | 31 | 34 |
| 15:00 | 14 | 5 | 66 | 227 | 101 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 422 | 32 | 34 |
| 16:00 | 16 | 10 | 93 | 238 | 74 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 439 | 31 | 34 |
| 17:00 | 11 | 2 | 78 | 205 | 66 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 366 | 31 | 33 |
| 18:00 | 7 | 1 | 38 | 147 | 53 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 251 | 31 | 34 |
| 19:00 | 5 | 2 | 38 | 130 | 37 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 215 | 31 | 33 |
| 20:00 | 1 | 1 | 41 | 93 | 36 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 173 | 31 | 33 |
| 21:00 | 2 | 4 | 24 | 68 | 17 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 117 | 30 | 33 |
| 22:00 | 0 | 0 | 12 | 45 | 19 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 78 | 32 | 34 |
| 23:00 | 0 | 0 | 3 | 23 | <u>17</u> 1090 | <u>1</u> 92 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 46 | 33 | 38 |
| Total | <u>179</u> 3.2% | 61 | 1149 | 3065 | | | 5 | <u> </u> | <u> </u> | 0.0% | 0.0% | 0.0% | 0.0% | 5643 | | |
| Percent AM Peak | 08:00 | <u> </u> | 20.4% | 54.3% | <u>19.3%</u> 11:00 | <u>1.6%</u> 08:00 | 0.1% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 11:00 | | |
| Vol. | 23 | 10.00 | 10:00 90 | 11:00 260 | 94 | 08.00 11 | 10.00 | | | | | | | 439 | | |
| PM Peak | 14:00 | 16:00 | 13:00 | 12:00 | 12:00 | 15:00 | 12:00 | 23:00 | 17:00 | | | | | 12:00 | | |
| Vol. | 21 | 10.00 | 106 | 270 | 12.00 | 15.00 | 12.00 | 23.00 | 17.00 | | | | | 497 | | |
| voi. | 21 | 10 | 100 | 270 | 102 | 9 | | | 1 | | | | | 497 | | |
| Grand | | | | | | | | | | | | | | | | |
| Total | 402 | 152 | 2275 | 6120 | 2119 | 171 | 11 | 2 | 1 | 0 | 0 | 0 | 0 | 11253 | | |
| Percent | 3.6% | 1.4% | 20.2% | 54.4% | 18.8% | 1.5% | 0.1% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | | | |
| | ,. | | th Percentile | | 22 MPH | | | ,. | ,. | ,. | ,. | ,. | ,. | | | |
| | | 501 | th Percentile | | 27 MPH | | | | | | | | | | | |
| | | | th Percentile | | 31 MPH | | | | | | | | | | | |
| | | 951 | th Percentile | | 34 MPH | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| Stats | | 10 MPH | Pace Speed | d: 21-3 | 0 MPH | | | | | | | | | | | |
| | Number | | s > 30 MPH | J · | 2304 | | | | | | | | | | | |
| | | | s > 30 MPF s > 30 MPF | | 2304 | | | | | | | | | | | |
| | | | ed(Average | | 20.3 % 27 MPH | | | | | | | | | | | |
| | | mean ope | culturelage | ,. 2 | _ / 1011 1 1 | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |

Cranston, Rhode Island

Dyer Avenue

(Source; RIDOT 1998 – 2019)



Cranston, Rhode Island

Traffic Volumes



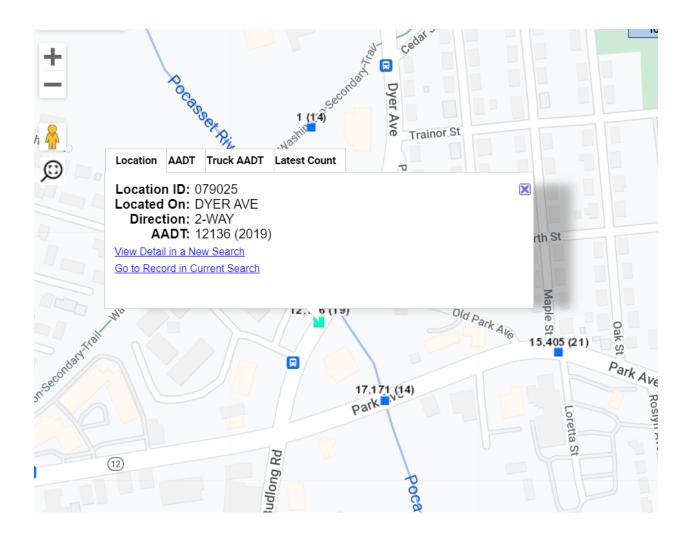
Dyer Ave, Cranston-Station 079025:

| AADT | ? | | | | | | |
|------|------|--------|--------|-----|-----|--------------|----------|
| | Year | AADT | DHV-30 | K % | D % | PA | BC |
| | 2019 | 12,136 | | | | 11,385 (94%) | 750 (6%) |

HISTORICAL DATA FROM STATION 070100(IN SAME AREA AS STATION 079025):

| | | 00 | PHIL | | | | | | | | | | | |
|------|---|----------------------------|--------|-------|------|--|---|----|---|--|--|--|--|--|
| Town | Town Roadway Segment StationNo AADT Date Bridge PeakHr Funcl Lo | | | | | | | | | | | | | |
| 07 | DYER AVE | CRANSTON ST & STHW 12 PARK | 070100 | 12200 | 1998 | | 7 | 16 | S | | | | | |
| 07 | DYER AVE | CRANSTON ST & STHW 12 PARK | 070100 | 8500 | 2008 | | 7 | 16 | S | | | | | |
| 07 | DYER AVE | CRANSTON ST & STHW 12 PARK | 070100 | 9300 | 2013 | | 7 | 16 | S | | | | | |

LOCATION OF STATION 079025



BETA Group, Inc. 701 George Washington Highway Lincoln, Rhode Island 02865 401.333.2382

| | 3/6/23 | 3/7/23 | 3/8/23 | 3/9/23 | 3/10/23 | Weekday | 3/11/23 | 3/12/23 |
|----------|--------|--------|--------|--------|---------|---------|---------|---------|
| Time | Mon | Tue | Wed | Thu | Fri | Average | Sat | Sun |
| 12:00 AM | * | * | 42 | 44 | 44 | 43 | 115 | 1 |
| 01:00 | * | * | 22 | 27 | 49 | 33 | 72 | ł |
| 02:00 | * | * | 9 | 27 | 22 | 19 | 45 | ł |
| 03:00 | * | * | 16 | 20 | 18 | 18 | 31 | ł. |
| 04:00 | * | * | 44 | 42 | 55 | 47 | 30 | ł |
| 05:00 | * | * | 147 | 142 | 158 | 149 | 56 | k |
| 06:00 | * | * | 281 | 285 | 290 | 285 | 126 | ÷ |
| 07:00 | * | * | 687 | 710 | 684 | 694 | 208 | * |
| 08:00 | * | * | 696 | 669 | 638 | 668 | 314 | * |
| 09:00 | * | * | 529 | 565 | 598 | 564 | 467 | ł. |
| 10:00 | * | * | 493 | 522 | 574 | 530 | 556 | * |
| 11:00 | * | 425 | 510 | 591 | 568 | 524 | 598 | ł. |
| 12:00 PM | * | 558 | 626 | 664 | 654 | 626 | 596 | * |
| 01:00 | * | 588 | 577 | 590 | 619 | 594 | 603 | × |
| 02:00 | * | 704 | 715 | 764 | 762 | 736 | 581 | × |
| 03:00 | * | 811 | 781 | 794 | 814 | 800 | 611 | ł. |
| 04:00 | * | 817 | 832 | 896 | 915 | 865 | 568 | k. |
| 05:00 | * | 734 | 765 | 733 | 770 | 750 | 486 | × |
| 06:00 | * | 553 | 581 | 550 | 574 | 564 | 503 | * |
| 07:00 | * | 385 | 462 | 440 | 495 | 446 | 411 | * |
| 08:00 | * | 309 | 314 | 330 | 397 | 338 | 333 | * |
| 09:00 | * | 272 | 259 | 276 | 320 | 282 | 158 | * |
| 10:00 | * | 172 | 166 | 186 | 276 | 200 | * | * |
| 11:00 | * | 102 | 96 | 104 | 183 | 121 | * | * |
| Total | 0 | 6430 | 9650 | 9971 | 10477 | 9896 | 7468 | C |
| Percent | 0.0% | 65.0% | 97.5% | 100.8% | 105.9% | | 75.5% | 0.0% |
| AM Peak | | 11:00 | 08:00 | 07:00 | 07:00 | 07:00 | 11:00 | |
| Volume | | 425 | 696 | 710 | 684 | 694 | 598 | |
| PM Peak | | 04:00 | 04:00 | 04:00 | 04:00 | 04:00 | 03:00 | |
| Volume | | 817 | 832 | 896 | 915 | 865 | 611 | |

Cranston, Rhode Island

Speeds



BETA Group, Inc. 701 George Washington Highway Lincoln, Rhode Island 02865 401.333.2382

| | 3/7/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
|---|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| | Time | MPH | | 25 MPH | 30 MPH | | | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| _ | 12:00 AM | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 1:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 2:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 3:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 4:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 5:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 6:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 7:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 8:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 9:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| | 11:00 | 0 | 5 | 20 | 68 | 85 | 12 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 192 |
| | 12:00 PM | 5 | 3 | 24 | 124 | 111 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 276 |
| | 1:00 | 0 | 1 | 30 | 135 | 115 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 299 |
| | 2:00 | 19 | 7 | 27 | 166 | 125 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 353 |
| | 3:00 | 6 | 8 | 70 | 194 | 133 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 425 |
| | 4:00 | 0 | 2 | 39 | 215 | 166 | 25 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 449 |
| | 5:00 | 0 | 3 | 39 | 190 | 148 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 397 |
| | 6:00 | 0 | 1 | 18 | 153 | 110 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 297 |
| | 7:00 | 0 | 0 | 23 | 104 | 88 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 225 |
| | 8:00 | 0 | 0 | 17 | 81 | 82 | 13 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 194 |
| | 9:00 | 0 | 1 | 6 | | 56 | 9 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 146 |
| | 10:00 | 1 | 0 | 7 | 37 | 41 | 9 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 99 |
| | 11:00 | 0 | 1 | 1 | 26 | 26 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 64 |
| | Total | 31 | 32 | 321 | 1564 | 1286 | 168 | 11 | 1 | 2 | 0 | 0 | 0 | 0 | 3416 |

BETA Group, Inc. 701 George Washington Highway Lincoln, Rhode Island 02865 401.333.2382

| | 1 | | | | | | | | | | | | | |
|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| 3/8/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
| Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| 12:00 AM | 0 | 0 | 0 | 7 | 13 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 23 |
| 1:00 | 0 | 0 | 1 | 2 | 4 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 2:00 | 0 | 0 | 0 | 2 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 3:00 | 0 | 0 | 1 | 4 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 4:00 | 0 | 1 | 0 | 9 | 7 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| 5:00 | 0 | 0 | 6 | 14 | 26 | 18 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 65 |
| 6:00 | 1 | 1 | 9 | 43 | 60 | 23 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 138 |
| 7:00 | 5 | 5 | 18 | 147 | 107 | 18 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 304 |
| 8:00 | 4 | 3 | 28 | 123 | 130 | 21 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 315 |
| 9:00 | 0 | 1 | 19 | 110 | 83 | 12 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 226 |
| 10:00 | 0 | 1 | 18 | 92 | 91 | 20 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 225 |
| 11:00 | 0 | 2 | 17 | 104 | 85 | 21 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 231 |
| 12:00 PM | 0 | 7 | 29 | 114 | 125 | 25 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 310 |
| 1:00 | 2 | 5 | 34 | 126 | 102 | 24 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 294 |
| 2:00 | 0 | 5 | 43 | 167 | 127 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 362 |
| 3:00 | 1 | 4 | 50 | 181 | 123 | 26 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 387 |
| 4:00 | 4 | 9 | 31 | 186 | 147 | 21 | 3 | 1 | 1 | 0 | 0 | 0 | 0 | 403 |
| 5:00 | 0 | 1 | 33 | 193 | 164 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 408 |
| 6:00 | 1 | 0 | 21 | 163 | 91 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 299 |
| 7:00 | 0 | 2 | 14 | 118 | 90 | 15 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 240 |
| 8:00 | 0 | 0 | 16 | 88 | 77 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 192 |
| 9:00 | 0 | 0 | 11 | 68 | 62 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 155 |
| 10:00 | 0 | 0 | 4 | 44 | 30 | 13 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 92 |
| 11:00 | 0 | 0 | 4 | 28 | 18 | 13 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 64 |
| Total | 18 | 47 | 407 | 2133 | 1767 | 368 | 39 | 3 | 1 | 0 | 0 | 0 | 0 | 4783 |
| | | | | | | | | | | | | | | |

BETA Group, Inc. 701 George Washington Highway Lincoln, Rhode Island 02865 401.333.2382

| | , | | | | | | | | | | | | | |
|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| 3/9/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
| Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| 12:00 AM | 0 | 0 | 2 | 12 | 9 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 29 |
| 1:00 | 0 | 0 | 1 | 3 | 4 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 2:00 | 0 | 0 | 0 | 5 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 3:00 | 0 | 0 | 1 | 6 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 4:00 | 0 | 0 | 0 | 5 | 11 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 19 |
| 5:00 | 0 | 0 | 7 | 15 | 29 | 12 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 64 |
| 6:00 | 6 | 3 | 6 | 39 | 54 | 26 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 138 |
| 7:00 | 0 | 7 | 40 | 90 | 156 | 36 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 332 |
| 8:00 | 5 | 7 | 22 | 123 | 144 | 32 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 338 |
| 9:00 | 2 | 2 | 14 | 130 | 103 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 270 |
| 10:00 | 8 | 3 | 27 | 118 | 92 | 34 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 285 |
| 11:00 | 13 | 12 | 47 | 112 | 96 | 22 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 304 |
| 12:00 PM | 1 | 1 | 26 | 167 | 153 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 368 |
| 1:00 | 0 | 4 | 26 | 132 | 144 | 26 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 334 |
| 2:00 | 89 | 5 | 68 | 167 | 90 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 430 |
| 3:00 | 0 | 9 | 74 | 175 | 137 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 413 |
| 4:00 | 0 | 3 | 76 | 216 | 157 | 19 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 474 |
| 5:00 | 3 | 3 | 45 | 161 | 145 | 23 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 385 |
| 6:00 | 1 | 0 | 20 | 126 | 119 | 17 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 284 |
| 7:00 | 0 | 5 | 25 | 92 | 92 | 10 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 227 |
| 8:00 | 0 | 0 | 17 | 95 | 68 | 18 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 202 |
| 9:00 | 0 | 0 | 12 | 73 | 71 | 8 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 167 |
| 10:00 | 0 | 0 | 9 | 53 | 51 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 126 |
| 11:00 | 0 | 0 | 1 | 18 | 30 | 12 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 62 |
| Total | 128 | 64 | 566 | 2133 | 1965 | 384 | 39 | 5 | 3 | 0 | 0 | 0 | 2 | 5289 |
| | | | | | | | | | | | | | | |

BETA Group, Inc. 701 George Washington Highway Lincoln, Rhode Island 02865 401.333.2382

| 3/10/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| Time | MPH | | 25 MPH | | 35 MPH | 40 MPH | | 50 MPH | | 60 MPH | | | MPH | Total |
| 12:00 AM | 0 | 0 | 3 | 6 | 11 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 1:00 | 0 | 0 | 0 | 11 | 10 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 2:00 | 0 | 0 | 0 | 2 | 3 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 8 |
| 3:00 | 0 | 0 | 0 | 5 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 4:00 | 0 | 0 | 0 | 2 | 13 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 5:00 | 0 | 0 | 6 | 17 | 22 | 13 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 63 |
| 6:00 | 3 | 3 | 2 | 36 | 61 | 30 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 140 |
| 7:00 | 6 | 7 | 34 | 119 | 107 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 304 |
| 8:00 | 4 | 4 | 40 | 100 | 114 | 30 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 296 |
| 9:00 | 0 | 1 | 12 | 101 | 106 | 28 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 250 |
| 10:00 | 17 | 18 | 25 | 111 | 94 | 34 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 300 |
| 11:00 | 0 | 3 | 22 | 95 | 106 | 36 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 266 |
| 12:00 PM | 4 | 6 | 32 | 150 | 122 | | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 345 |
| 1:00 | 1 | 1 | 22 | 149 | 130 | 23 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 327 |
| 2:00 | 0 | 5 | 55 | 161 | 162 | 25 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 409 |
| 3:00 | 1 | 9 | 51 | 188 | 147 | 33 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 434 |
| 4:00 | 5 | 8 | 65 | 209 | 150 | | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 465 |
| 5:00 | 0 | 4 | 33 | 206 | 152 | 21 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 418 |
| 6:00 | 0 | 0 | 32 | 143 | 126 | 18 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 320 |
| 7:00 | 0 | 4 | 18 | 135 | 106 | 20 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 284 |
| 8:00 | 0 | 2 | 7 | 93 | 102 | 15 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 220 |
| 9:00 | 0 | 1 | 10 | 91 | 67 | 15 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 187 |
| 10:00 | 0 | 0 | 10 | 61 | 74 | 18 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 166 |
| 11:00 | 0 | 0 | - | 45 | 55 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 117 |
| Total | 41 | 76 | 487 | 2236 | 2044 | 466 | 40 | 9 | 1 | 0 | 0 | 0 | 0 | 5400 |

BETA Group, Inc. 701 George Washington Highway Lincoln, Rhode Island 02865 401.333.2382

Direction: North, Lane 1

| 3/11/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
|-------------|--------|----------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| 12:00 AM | 0 | 0 | 3 | 21 | 29 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 59 |
| 1:00 | 0 | 0 | 3 | 13 | 18 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 37 |
| 2:00 | 0 | 0 | 0 | 6 | 9 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 16 |
| 3:00 | 0 | 0 | 1 | 3 | 5 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 13 |
| 4:00 | 0 | 1 | 0 | 3 | 10 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 18 |
| 5:00 | 1 | 0 | 1 | 9 | 12 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 28 |
| 6:00 | 0 | 1 | 3 | 17 | 26 | 13 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 62 |
| 7:00 | 0 | 3 | 3 | 18 | 40 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 75 |
| 8:00 | 0 | 0 | 7 | 40 | 62 | 14 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 126 |
| 9:00 | 0 | 4 | 22 | 77 | 91 | 21 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 221 |
| 10:00 | 0 | 17 | 17 | 88 | 125 | 18 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 268 |
| 11:00 | 0 | 0 | 16 | 84 | 142 | 30 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 273 |
| 12:00 PM | 1 | 0 | 16 | 120 | 139 | 21 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 301 |
| 1:00 | 0 | 5 | 26 | 128 | 119 | 31 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 313 |
| 2:00 | 1 | 13 | 31 | 155 | 85 | 26 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 312 |
| 3:00 | 8 | 2 | 21 | 141 | 116 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 311 |
| 4:00 | 0 | 2 | 23 | 99 | 139 | 27 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 296 |
| 5:00 | 0 | 0 | 8 | 108 | 139 | 20 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 278 |
| 6:00 | 0 | 0 | 40 | 106 | 102 | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 260 |
| 7:00 | 0 | 1 | 14 | 120 | 81 | 17 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 234 |
| 8:00 | 0 | 0 | 10 | 72 | 82 | 27 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 193 |
| 9:00 | 0 | 0 | 9 | 54 | 43 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 108 |
| 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| 11:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| Total | 11 | 49 | 274 | 1482 | 1614 | 325 | 41 | 5 | 1 | 0 | 0 | 0 | 0 | 3802 |
| Grand Total | 229 | 268 | 2055 | 9548 | 8676 | 1711 | 170 | 23 | 8 | 0 | 0 | 0 | 2 | 22690 |
| Stats | | | Percentile | 15th | 50th | 85th | 95th | | | | | | | |
| | | | Speed | 26 | 30 | 34 | 36 | | | | | | | |
| | Me | an Speed | (Average) | 29.6 | | | | | | | | | | |

Mean Speed (Average) 29.6 10 MPH Pace Speed 25-34 Number in Pace 18092 Percent in Pace 79.7% Number > 25 MPH 20140 Percent > 25 MPH 88.8%

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| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | _ | | , | | | | | | | | | | | | | |
|---|---|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 3/7/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 12:00 AM | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 1:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 2:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 3:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 4:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 5:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 6:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 7:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 8:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 9:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| 12:00 PM 2 3 20 117 105 35 0 0 0 0 0 0 0 282 1:00 3 4 13 96 121 44 5 1 0 0 0 1 1 289 2:00 0 0 24 143 140 39 4 1 0 0 0 0 351 3:00 1 7 42 146 142 44 4 0 0 0 0 0 386 4:00 1 16 143 156 47 4 0 0 0 0 0 376 5:00 0 2 36 120 147 27 4 1 0 0 0 0 337 6:00 2 2 14 112 102 21 3 0 0 0 0 0 256 7:00 1 0 6 56 69 24 | | 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | 0 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 11:00 | 1 | 6 | 19 | 80 | 99 | 23 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 233 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 12:00 PM | 2 | 3 | 20 | 117 | 105 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 282 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 1:00 | 3 | 4 | 13 | 96 | 121 | 44 | 5 | 1 | 0 | 0 | 0 | 1 | 1 | 289 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 2:00 | 0 | 0 | 24 | 143 | 140 | 39 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 351 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 3:00 | 1 | 7 | 42 | 146 | 142 | 44 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 386 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 4:00 | 1 | 1 | 16 | 143 | 156 | 47 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 368 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 5:00 | 0 | 2 | 36 | 120 | 147 | 27 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 337 |
| 8:00 0 1 12 27 55 18 2 0 0 0 0 0 115 9:00 0 0 5 39 62 19 1 0 0 0 0 0 126 10:00 0 1 1 12 31 21 5 1 1 0 0 0 0 73 11:00 0 0 1 5 21 10 1 0 0 0 0 38 | | 6:00 | 2 | 2 | 14 | 112 | 102 | 21 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 256 |
| 9:00 0 0 5 39 62 19 1 0 0 0 0 0 126 10:00 0 1 1 12 31 21 5 1 1 0 0 0 0 73 11:00 0 0 1 5 21 10 1 0 0 0 0 38 | | 7:00 | 1 | 0 | 6 | 56 | 69 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 160 |
| 10:00 0 1 1 12 31 21 5 1 1 0 0 0 73 11:00 0 0 1 5 21 10 1 0 0 0 0 38 | | 8:00 | 0 | 1 | 12 | 27 | 55 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 115 |
| <u>11:00 0 0 1 5 21 10 1 0 0 0 0 0 38</u> | | 9:00 | 0 | 0 | 5 | 39 | 62 | 19 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 126 |
| | | 10:00 | 0 | 1 | 1 | 12 | 31 | 21 | 5 | 1 | 1 | 0 | 0 | 0 | 0 | 73 |
| Total 11 27 209 1096 1250 372 41 4 1 1 0 1 1 3014 | | 11:00 | 0 | 0 | 1 | 5 | 21 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 38 |
| | | Total | 11 | 27 | 209 | 1096 | 1250 | 372 | 41 | 4 | 1 | 1 | 0 | 1 | 1 | 3014 |

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| _ | | | | | | | | | | | | | | | |
|---|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| | 3/8/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
| _ | Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| | 12:00 AM | 0 | 0 | 0 | 3 | 11 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| | 1:00 | 0 | 0 | 1 | 1 | 5 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 10 |
| | 2:00 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| | 3:00 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| | 4:00 | 0 | 0 | 0 | 1 | 10 | 9 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| | 5:00 | 0 | 2 | 5 | 19 | 28 | 19 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 82 |
| | 6:00 | 0 | 0 | 9 | 36 | 68 | 23 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 143 |
| | 7:00 | 2 | 2 | 27 | 133 | 171 | 41 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 383 |
| | 8:00 | 7 | 1 | 22 | 129 | 166 | 53 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 381 |
| | 9:00 | 2 | 4 | 8 | 110 | 141 | 33 | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 303 |
| | 10:00 | 0 | 6 | 14 | 86 | 115 | 41 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 268 |
| | 11:00 | 2 | 2 | 11 | 90 | 128 | 36 | 9 | 0 | 0 | 1 | 0 | 0 | 0 | 279 |
| | 12:00 PM | 1 | 1 | 18 | 90 | 157 | 46 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 316 |
| | 1:00 | 3 | 5 | 21 | 94 | 119 | 33 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 283 |
| | 2:00 | 1 | 2 | 13 | 129 | 143 | 61 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 353 |
| | 3:00 | 0 | 1 | 39 | 124 | 163 | 59 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 394 |
| | 4:00 | 2 | 6 | 26 | 155 | 183 | 51 | 5 | 0 | 0 | 0 | 0 | 1 | 0 | 429 |
| | 5:00 | 0 | 6 | 27 | 144 | 138 | 34 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 357 |
| | 6:00 | 0 | 5 | 10 | 100 | 131 | 30 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 282 |
| | 7:00 | 0 | 1 | 7 | 69 | 99 | 38 | 6 | 0 | 1 | 0 | 0 | 0 | 1 | 222 |
| | 8:00 | 0 | 0 | 11 | 40 | 51 | 19 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 122 |
| | 9:00 | 0 | 0 | 9 | 32 | 35 | 27 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 104 |
| | 10:00 | 0 | 0 | 7 | 26 | 29 | 9 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 74 |
| | 11:00 | 0 | 0 | 1 | 5 | 13 | 12 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 32 |
| _ | Total | 20 | 44 | 286 | 1618 | 2106 | 685 | 87 | 11 | 4 | 1 | 2 | 2 | 1 | 4867 |
| | | | | | | | | | | | | | | | |

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| | , | | | | | | | | | | | | | |
|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| 3/9/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
| Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| 12:00 AM | 0 | 0 | 0 | 2 | 7 | 2 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 15 |
| 1:00 | 0 | 0 | 0 | 6 | 4 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 2:00 | 0 | 0 | 1 | 2 | 7 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| 3:00 | 0 | 0 | 0 | 1 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 4:00 | 0 | 0 | 1 | 2 | 10 | 7 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 23 |
| 5:00 | 0 | 0 | 7 | 16 | 32 | 15 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 78 |
| 6:00 | 0 | 0 | 4 | 37 | 72 | 29 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 147 |
| 7:00 | 18 | 12 | 17 | 100 | 161 | 57 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 378 |
| 8:00 | 2 | 4 | 17 | 97 | 153 | 53 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 331 |
| 9:00 | 5 | 7 | 22 | 85 | 118 | 50 | 7 | 0 | 0 | 0 | 0 | 1 | 0 | 295 |
| 10:00 | 3 | 5 | 16 | 83 | 98 | 25 | 5 | 1 | 1 | 0 | 0 | 0 | 0 | 237 |
| 11:00 | 7 | 32 | 53 | 90 | 79 | 25 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 287 |
| 12:00 PM | 0 | 5 | 23 | 119 | 110 | 36 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 296 |
| 1:00 | 0 | 3 | 11 | 98 | 111 | 31 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 256 |
| 2:00 | 1 | 13 | 34 | 105 | 139 | 34 | 6 | 1 | 0 | 1 | 0 | 0 | 0 | 334 |
| 3:00 | 3 | 1 | 31 | 157 | 125 | 56 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 381 |
| 4:00 | 0 | 4 | 30 | 136 | 197 | 49 | 5 | 0 | 0 | 0 | 0 | 1 | 0 | 422 |
| 5:00 | 3 | 4 | 14 | 132 | 147 | 43 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 348 |
| 6:00 | 0 | 1 | 18 | 117 | 112 | 16 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 266 |
| 7:00 | 0 | 0 | 2 | 58 | 123 | 26 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 213 |
| 8:00 | 0 | 0 | 6 | 35 | 70 | 13 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 128 |
| 9:00 | 0 | 0 | 4 | 40 | 44 | 15 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 109 |
| 10:00 | 0 | 0 | 2 | 20 | 21 | 13 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 60 |
| 11:00 | 0 | 0 | 0 | 9 | 21 | 11 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 42 |
| Total | 42 | 91 | 313 | 1547 | 1966 | 612 | 93 | 6 | 3 | 3 | 3 | 2 | 1 | 4682 |
| | | | | | | | | | | | | | | |

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| | 1 | | | | | | | | | | | | | |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| 3/10/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
| Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| 12:00 AM | 0 | 0 | 0 | 3 | 7 | 8 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 20 |
| 1:00 | 0 | 0 | 0 | 3 | 11 | 8 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 25 |
| 2:00 | 0 | 0 | 0 | 2 | 6 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 14 |
| 3:00 | 0 | 0 | 0 | 2 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 4:00 | 0 | 1 | 2 | 4 | 9 | 12 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 31 |
| 5:00 | 0 | 0 | 12 | 17 | 30 | 22 | 11 | 1 | 1 | 0 | 0 | 1 | 0 | 95 |
| 6:00 | 2 | 2 | 5 | 36 | 71 | 30 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 150 |
| 7:00 | 0 | 0 | 30 | 135 | 159 | 49 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 380 |
| 8:00 | 0 | 0 | 12 | 129 | 144 | 48 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 342 |
| 9:00 | 1 | 3 | 30 | 126 | 143 | 40 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 348 |
| 10:00 | 6 | 1 | 17 | 83 | 123 | 36 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 274 |
| 11:00 | 1 | 2 | 18 | 108 | 125 | 39 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 302 |
| 12:00 PM | 2 | 1 | 5 | 96 | 158 | 43 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 309 |
| 1:00 | 0 | 6 | 17 | 87 | 125 | 49 | 5 | 2 | 0 | 0 | 0 | 0 | 1 | 292 |
| 2:00 | 0 | 1 | 32 | 118 | 150 | 42 | 5 | 2 | 2 | 0 | 0 | 0 | 1 | 353 |
| 3:00 | 1 | 2 | 18 | 152 | 158 | 44 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 380 |
| 4:00 | 0 | 1 | 31 | 178 | 188 | 44 | 6 | 1 | 0 | 1 | 0 | 0 | 0 | 450 |
| 5:00 | 0 | 1 | 17 | 120 | 154 | 56 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 352 |
| 6:00 | 0 | 1 | 17 | 92 | 124 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 254 |
| 7:00 | 0 | 0 | 7 | 63 | 107 | 33 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 211 |
| 8:00 | 0 | 0 | 4 | 59 | 85 | 26 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 177 |
| 9:00 | 0 | 1 | 8 | 34 | 57 | 29 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 133 |
| 10:00 | 0 | 0 | 1 | 38 | 43 | 21 | 4 | 1 | 1 | 1 | 0 | 0 | 0 | 110 |
| 11:00 | 0 | 0 | 2 | 20 | 29 | 12 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 66 |
| Total | 13 | 23 | 285 | 1705 | 2210 | 715 | 92 | 23 | 5 | 3 | 0 | 1 | 2 | 5077 |
| | | | | | | | | | | | | | | |

BETA Group, Inc. 701 George Washington Highway Lincoln, Rhode Island 02865 401.333.2382

| niection. Souti | i, Lane z | | | | | | | | | | | | | |
|-----------------|-----------|----------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|
| 3/11/2023 | 0 - 15 | > 15 - | > 20 - | > 25 - | > 30 - | > 35 - | > 40 - | > 45 - | > 50 - | > 55 - | > 60 - | > 65 - | > 70 | |
| Time | MPH | 20 MPH | 25 MPH | 30 MPH | 35 MPH | 40 MPH | 45 MPH | 50 MPH | 55 MPH | 60 MPH | 65 MPH | 70 MPH | MPH | Total |
| 12:00 AM | 0 | 0 | 2 | 11 | 19 | 18 | 4 | 1 | 1 | 0 | 0 | 0 | 0 | 56 |
| 1:00 | 0 | 0 | 0 | 4 | 17 | 10 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 35 |
| 2:00 | 0 | 0 | 1 | 6 | 7 | 9 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 29 |
| 3:00 | 0 | 0 | 0 | 2 | 10 | 3 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 18 |
| 4:00 | 0 | 0 | 1 | 5 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 5:00 | 0 | 0 | 1 | 11 | 9 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 |
| 6:00 | 0 | 0 | 2 | 15 | 26 | 17 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 64 |
| 7:00 | 0 | 0 | 3 | 27 | 72 | 25 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 133 |
| 8:00 | 0 | 0 | 5 | 59 | 70 | 43 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 188 |
| 9:00 | 0 | 0 | 13 | 89 | 107 | 28 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 246 |
| 10:00 | 1 | 4 | 21 | 82 | 113 | 57 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 288 |
| 11:00 | 0 | 1 | 16 | 103 | 154 | 48 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 325 |
| 12:00 PM | 0 | 1 | 10 | 97 | 134 | 47 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 295 |
| 1:00 | 0 | 0 | 9 | 74 | 145 | 49 | 11 | 1 | 1 | 0 | 0 | 0 | 0 | 290 |
| 2:00 | 0 | 0 | 15 | 82 | 122 | 43 | 5 | 1 | 0 | 1 | 0 | 0 | 0 | 269 |
| 3:00 | 0 | 1 | 28 | 105 | 118 | 42 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 300 |
| 4:00 | 0 | 0 | 13 | 88 | 120 | 47 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 272 |
| 5:00 | 0 | 0 | 5 | 54 | 99 | 42 | 6 | 0 | 0 | 1 | 1 | 0 | 0 | 208 |
| 6:00 | 0 | 0 | 14 | 77 | 116 | 32 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 243 |
| 7:00 | 0 | 1 | 8 | 52 | 79 | 26 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 177 |
| 8:00 | 0 | 1 | 7 | 28 | 74 | 23 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 140 |
| 9:00 | 0 | 0 | 3 | 15 | 24 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 50 |
| 10:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | C |
| 11:00 | * | * | * | * | * | * | * | * | * | * | * | * | * | C |
| Total | 1 | 9 | 177 | 1086 | 1638 | 626 | 107 | 11 | 5 | 4 | 1 | 1 | 0 | 3666 |
| Grand Total | 87 | 194 | 1270 | 7052 | 9170 | 3010 | 420 | 55 | 18 | 12 | 6 | 7 | 5 | 21306 |
| Stats | | | Percentile | 15th | 50th | 85th | 95th | | | | | | | |
| | | | Speed | 27 | 31 | 35 | 38 | | | | | | | |
| | Mea | an Speed | (Average) | 31.1 | | | | | | | | | | |
| | | | | | | | | | | | | | | |

10 MPH Pace Speed 25-34

Number in Pace 16064 Percent in Pace 75.4% Number > 25 MPH 19754

Percent > 25 MPH 92.7%

Cranston, Rhode Island

A

Intersection Turning Movement Count

Cranston Street at Dyer Avenue



Cranston, Rhode Island

Cranston Street at Dyer Avenue

(Source; Vanasse & Associates, January 2023)



N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | | | Grou | ups Printe | d- Cars & | & Peds - | Trucks & | & Buses - | Bikes by | v Directi | on | | | | | |
|----------------------|-------|---------|-------|------|------------|-----------|----------|----------|-----------|----------|-----------|------|-------|----------|--------|------|------------|
| | | Dyer Av | venue | | 1 | Cranston | | | | Dyer A | | | (| Cranston | Street | | |
| | | From N | Jorth | | | From 1 | East | | | From S | outh | | | From V | West | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 07:00 AM | 24 | 51 | 5 | 0 | 8 | 45 | 11 | 0 | 23 | 23 | 1 | 0 | 0 | 62 | 13 | 0 | 266 |
| 07:15 AM | 22 | 62 | 8 | 0 | 7 | 63 | 13 | 0 | 19 | 32 | 3 | 0 | 4 | 77 | 22 | 0 | 332 |
| 07:30 AM | 25 | 69 | 10 | 1 | 9 | 61 | 19 | 1 | 21 | 61 | 9 | 1 | 7 | 80 | 28 | 0 | 402 |
| 07:45 AM | 50 | 105 | 6 | 0 | 8 | 81 | 31 | 0 | 33 | 50 | 9 | 0 | 5 | 82 | 36 | 0 | 496 |
| Total | 121 | 287 | 29 | 1 | 32 | 250 | 74 | 1 | 96 | 166 | 22 | 1 | 16 | 301 | 99 | 0 | 1496 |
| | I. | | | | | | | | | | | | | | | | |
| 08:00 AM | 21 | 73 | 5 | 0 | 14 | 72 | 22 | 0 | 39 | 80 | 9 | 0 | 6 | 102 | 30 | 0 | 473 |
| 08:15 AM | 18 | 59 | 9 | 0 | 7 | 62 | 23 | 0 | 19 | 52 | 5 | 1 | 3 | 79 | 23 | 0 | 360 |
| 08:30 AM | 22 | 55 | 11 | 0 | 9 | 82 | 27 | 0 | 14 | 39 | 2 | 0 | 6 | 70 | 38 | 0 | 375 |
| 08:45 AM | 27 | 66 | 13 | 1 | 15 | 69 | 20 | 0 | 29 | 49 | 3 | 0 | 5 | 66 | 17 | 0 | 380 |
| Total | 88 | 253 | 38 | 1 | 45 | 285 | 92 | 0 | 101 | 220 | 19 | 1 | 20 | 317 | 108 | 0 | 1588 |
| | 1 | | | | | | | | | | | | | | | | |
| Grand Total | 209 | 540 | 67 | 2 | 77 | 535 | 166 | 1 | 197 | 386 | 41 | 2 | 36 | 618 | 207 | 0 | 3084 |
| Apprch % | 25.6 | 66 | 8.2 | 0.2 | 9.9 | 68.7 | 21.3 | 0.1 | 31.5 | 61.7 | 6.5 | 0.3 | 4.2 | 71.8 | 24 | 0 | |
| Total % | 6.8 | 17.5 | 2.2 | 0.1 | 2.5 | 17.3 | 5.4 | 0 | 6.4 | 12.5 | 1.3 | 0.1 | 1.2 | 20 | 6.7 | 0 | |
| Cars & Peds | 202 | 528 | 66 | 2 | 76 | 522 | 160 | 1 | 192 | 376 | 41 | 2 | 35 | 610 | 204 | 0 | 3017 |
| % Cars & Peds | 96.7 | 97.8 | 98.5 | 100 | 98.7 | 97.6 | 96.4 | 100 | 97.5 | 97.4 | 100 | 100 | 97.2 | 98.7 | 98.6 | 0 | 97.8 |
| Trucks & Buses | 7 | 12 | 1 | 0 | 1 | 13 | 6 | 0 | 5 | 10 | 0 | 0 | 1 | 8 | 3 | 0 | 67 |
| % Trucks & Buses | 3.3 | 2.2 | 1.5 | 0 | 1.3 | 2.4 | 3.6 | 0 | 2.5 | 2.6 | 0 | 0 | 2.8 | 1.3 | 1.4 | 0 | 2.2 |
| Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| | | - | er Ave | | | | | nston St | | | | 2 | ver Aver | | | | | iston St | | | |
|----------------------|--------|---------|---------|----------|------------|-------|------|----------|------|------------|-------|------|----------|------|------------|-------|------|----------|------|------------|------------|
| | | Fi | rom No | rth | | | F | rom Ea | st | | | Fr | om Sou | ıth | | | F | rom We | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | | | | | | | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins at | : 07:30 A | M | | | | | | | | | | | | | | | |
| 07:30 AM | 25 | 69 | 10 | 1 | 105 | 9 | 61 | 19 | 1 | 90 | 21 | 61 | 9 | 1 | 92 | 7 | 80 | 28 | 0 | 115 | 402 |
| 07:45 AM | 50 | 105 | 6 | 0 | 161 | 8 | 81 | 31 | 0 | 120 | 33 | 50 | 9 | 0 | 92 | 5 | 82 | 36 | 0 | 123 | 496 |
| 08:00 AM | 21 | 73 | 5 | 0 | 99 | 14 | 72 | 22 | 0 | 108 | 39 | 80 | 9 | 0 | 128 | 6 | 102 | 30 | 0 | 138 | 473 |
| 08:15 AM | 18 | 59 | 9 | 0 | 86 | 7 | 62 | 23 | 0 | 92 | 19 | 52 | 5 | 1 | 77 | 3 | 79 | 23 | 0 | 105 | 360 |
| Total Volume | 114 | 306 | 30 | 1 | 451 | 38 | 276 | 95 | 1 | 410 | 112 | 243 | 32 | 2 | 389 | 21 | 343 | 117 | 0 | 481 | 1731 |
| % App. Total | 25.3 | 67.8 | 6.7 | 0.2 | | 9.3 | 67.3 | 23.2 | 0.2 | | 28.8 | 62.5 | 8.2 | 0.5 | | 4.4 | 71.3 | 24.3 | 0 | | |
| PHF | .570 | .729 | .750 | .250 | .700 | .679 | .852 | .766 | .250 | .854 | .718 | .759 | .889 | .500 | .760 | .750 | .841 | .813 | .000 | .871 | .872 |
| Cars & Peds | 111 | 302 | 29 | 1 | 443 | 38 | 272 | 91 | 1 | 402 | 109 | 238 | 32 | 2 | 381 | 20 | 339 | 117 | 0 | 476 | 1702 |
| % Cars & Peds | 97.4 | 98.7 | 96.7 | 100 | 98.2 | 100 | 98.6 | 95.8 | 100 | 98.0 | 97.3 | 97.9 | 100 | 100 | 97.9 | 95.2 | 98.8 | 100 | 0 | 99.0 | 98.3 |
| Trucks & Buses | 3 | 4 | 1 | 0 | 8 | 0 | 4 | 4 | 0 | 8 | 3 | 5 | 0 | 0 | 8 | 1 | 4 | 0 | 0 | 5 | 29 |
| % Trucks & Buses | 2.6 | 1.3 | 3.3 | 0 | 1.8 | 0 | 1.4 | 4.2 | 0 | 2.0 | 2.7 | 2.1 | 0 | 0 | 2.1 | 4.8 | 1.2 | 0 | 0 | 1.0 | 1.7 |
| Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | | | | | G | roups Pr | inted- Ca | ars & Ped | ls | | | | | | | |
|-------------|-------|---------|-------|------|-------|----------|----------|-----------|-----------|---------|-------|------|-------|----------|--------|------|------------|
| | | Dyer Av | /enue | | (| Cranston | Street | | | Dyer Av | venue | | (| Cranston | Street | | |
| | | From N | lorth | | | From | East | | | From S | outh | | | From | West | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 07:00 AM | 24 | 47 | 5 | 0 | 7 | 44 | 11 | 0 | 23 | 20 | 1 | 0 | 0 | 60 | 13 | 0 | 255 |
| 07:15 AM | 20 | 60 | 8 | 0 | 7 | 59 | 13 | 0 | 18 | 32 | 3 | 0 | 4 | 76 | 21 | 0 | 321 |
| 07:30 AM | 24 | 69 | 10 | 1 | 9 | 60 | 18 | 1 | 21 | 60 | 9 | 1 | 7 | 78 | 28 | 0 | 396 |
| 07:45 AM | 49 | 102 | 5 | 0 | 8 | 80 | 31 | 0 | 30 | 49 | 9 | 0 | 5 | 81 | 36 | 0 | 485 |
| Total | 117 | 278 | 28 | 1 | 31 | 243 | 73 | 1 | 92 | 161 | 22 | 1 | 16 | 295 | 98 | 0 | 1457 |
| | | | | | | | | | | | | | | | | | |
| 08:00 AM | 20 | 73 | 5 | 0 | 14 | 72 | 22 | 0 | 39 | 79 | 9 | 0 | 5 | 101 | 30 | 0 | 469 |
| 08:15 AM | 18 | 58 | 9 | 0 | 7 | 60 | 20 | 0 | 19 | 50 | 5 | 1 | 3 | 79 | 23 | 0 | 352 |
| 08:30 AM | 21 | 54 | 11 | 0 | 9 | 80 | 26 | 0 | 14 | 39 | 2 | 0 | 6 | 69 | 37 | 0 | 368 |
| 08:45 AM | 26 | 65 | 13 | 1 | 15 | 67 | 19 | 0 | 28 | 47 | 3 | 0 | 5 | 66 | 16 | 0 | 371 |
| Total | 85 | 250 | 38 | 1 | 45 | 279 | 87 | 0 | 100 | 215 | 19 | 1 | 19 | 315 | 106 | 0 | 1560 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 202 | 528 | 66 | 2 | 76 | 522 | 160 | 1 | 192 | 376 | 41 | 2 | 35 | 610 | 204 | 0 | 3017 |
| Apprch % | 25.3 | 66.2 | 8.3 | 0.3 | 10 | 68.8 | 21.1 | 0.1 | 31.4 | 61.5 | 6.7 | 0.3 | 4.1 | 71.8 | 24 | 0 | |
| Total % | 6.7 | 17.5 | 2.2 | 0.1 | 2.5 | 17.3 | 5.3 | 0 | 6.4 | 12.5 | 1.4 | 0.1 | 1.2 | 20.2 | 6.8 | 0 | |

| | | 2 | er Ave om No | | | | | nston St rom Ea | | | | 2 | er Ave om Sou | | | | | nston St rom We | | | |
|---------------|----------|----------|-----------------|---------|------------|--------|------|--------------------|------|------------|-------|------|------------------|------|------------|-------|------|--------------------|------|------------|------------|
| Start Time | Right | | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis I | From 07 | 7:00 AN | A to 08 | :45 AM - | Peak 1 | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Intersec | ction B | egins a | t 07:30 A | М | | | | | | | | | | | | | | | |
| 07:30 AM | 24 | 69 | 10 | 1 | 104 | 9 | 60 | 18 | 1 | 88 | 21 | 60 | 9 | 1 | 91 | 7 | 78 | 28 | 0 | 113 | 396 |
| 07:45 AM | 49 | 102 | 5 | 0 | 156 | 8 | 80 | 31 | 0 | 119 | 30 | 49 | 9 | 0 | 88 | 5 | 81 | 36 | 0 | 122 | 485 |
| 08:00 AM | 20 | 73 | 5 | 0 | 98 | 14 | 72 | 22 | 0 | 108 | 39 | 79 | 9 | 0 | 127 | 5 | 101 | 30 | 0 | 136 | 469 |
| 08:15 AM | 18 | 58 | 9 | 0 | 85 | 7 | 60 | 20 | 0 | 87 | 19 | 50 | 5 | 1 | 75 | 3 | 79 | 23 | 0 | 105 | 352 |
| Total Volume | 111 | 302 | 29 | 1 | 443 | 38 | 272 | 91 | 1 | 402 | 109 | 238 | 32 | 2 | 381 | 20 | 339 | 117 | 0 | 476 | 1702 |
| % App. Total | 25.1 | 68.2 | 6.5 | 0.2 | | 9.5 | 67.7 | 22.6 | 0.2 | | 28.6 | 62.5 | 8.4 | 0.5 | | 4.2 | 71.2 | 24.6 | 0 | | |
| PHF | .566 | .740 | .725 | .250 | .710 | .679 | .850 | .734 | .250 | .845 | .699 | .753 | .889 | .500 | .750 | .714 | .839 | .813 | .000 | .875 | .877 |

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | | | | | Gro | ups Prin | ted- True | cks & Bu | ses | | | | | | | |
|-------------|-------|---------|-------|------|-------|----------|----------|-----------|----------|---------|-------|------|-------|----------|--------|------|------------|
| | | Dyer Av | venue | | (| Cranston | Street | | | Dyer Av | venue | | (| Cranston | Street | | |
| | | From N | lorth | | | From I | East | | | From S | outh | | | From | West | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 07:00 AM | 0 | 4 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 0 | 11 |
| 07:15 AM | 2 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 11 |
| 07:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 6 |
| 07:45 AM | 1 | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 11 |
| Total | 4 | 9 | 1 | 0 | 1 | 7 | 1 | 0 | 4 | 5 | 0 | 0 | 0 | 6 | 1 | 0 | 39 |
| | | | | | | | | | | | | | | | | | |
| 08:00 AM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 4 |
| 08:15 AM | 0 | 1 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 08:30 AM | 1 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 7 |
| 08:45 AM | 1 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 9 |
| Total | 3 | 3 | 0 | 0 | 0 | 6 | 5 | 0 | 1 | 5 | 0 | 0 | 1 | 2 | 2 | 0 | 28 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 7 | 12 | 1 | 0 | 1 | 13 | 6 | 0 | 5 | 10 | 0 | 0 | 1 | 8 | 3 | 0 | 67 |
| Apprch % | 35 | 60 | 5 | 0 | 5 | 65 | 30 | 0 | 33.3 | 66.7 | 0 | 0 | 8.3 | 66.7 | 25 | 0 | |
| Total % | 10.4 | 17.9 | 1.5 | 0 | 1.5 | 19.4 | 9 | 0 | 7.5 | 14.9 | 0 | 0 | 1.5 | 11.9 | 4.5 | 0 | |

| | | Dy | er Ave | nue | | | Cra | ston St | reet | | | Dy | er Ave | nue | | | Crar | ston St | reet | | |
|---------------|----------|---------|---------|---------|------------|--------|------|---------|------|------------|-------|------|--------|------|------------|-------|------|---------|------|------------|------------|
| | | Fı | om No | rth | | | F | rom Ea | st | | | Fr | om Sou | ıth | | | F | rom We | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis I | From 07 | 7:00 AN | A to 08 | :45 AM - | Peak 1 | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins a | t 07:00 A | М | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 4 | 0 | 0 | 4 | 1 | 1 | 0 | 0 | 2 | 0 | 3 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 2 | 11 |
| 07:15 AM | 2 | 2 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 2 | 11 |
| 07:30 AM | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 6 |
| 07:45 AM | 1 | 3 | 1 | 0 | 5 | 0 | 1 | 0 | 0 | 1 | 3 | 1 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 1 | 11 |
| Total Volume | 4 | 9 | 1 | 0 | 14 | 1 | 7 | 1 | 0 | 9 | 4 | 5 | 0 | 0 | 9 | 0 | 6 | 1 | 0 | 7 | 39 |
| % App. Total | 28.6 | 64.3 | 7.1 | 0 | | 11.1 | 77.8 | 11.1 | 0 | | 44.4 | 55.6 | 0 | 0 | | 0 | 85.7 | 14.3 | 0 | | |
| PHF | .500 | .563 | .250 | .000 | .700 | .250 | .438 | .250 | .000 | .563 | .333 | .417 | .000 | .000 | .563 | .000 | .750 | .250 | .000 | .875 | .886 |

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | | | | | Grou | ps Printe | ed- Bike | s by Direc | ction | | | | | | | |
|-------------|-------|---------|-------|------|-------|----------|-----------|----------|------------|---------|-------|------|-------|----------|--------|------|------------|
| | | Dyer Av | venue | | (| Cranston | Street | | - | Dyer Av | /enue | | (| Cranston | Street | | |
| | | From N | lorth | | | From H | East | | | From S | outh | | | From V | West | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Total % | | | | | | | | | | | | | | | | | |

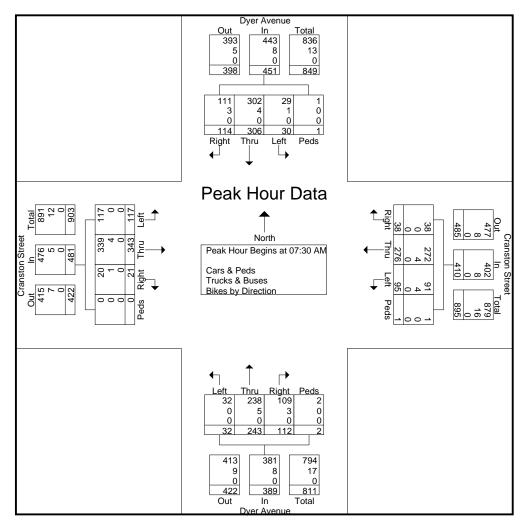
| | | Dy | er Ave | nue | | | Crar | ston St | reet | | | Dy | er Ave | nue | | | Crar | iston St | treet | | 1 |
|---------------|----------|---------|---------|----------|------------|--------|--------|---------|------|------------|-------|------|--------|------|------------|-------|------|----------|-------|------------|------------|
| | | Fı | om No | rth | | | F | rom Ea | st | | | Fr | om So | uth | | | F | rom We | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis F | From 07 | 7:00 AN | A to 08: | :45 AM - | Peak 1 | l of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins at | t 07:00 A | М | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % App. Total | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

Transportation Data Corporation

Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | 2 | ver Ave | | | | | iston S | | | | 2 | ver Ave | | | | | iston S | | | |
|----------------------|----------|---------|--------------|------------|------------|--------|------|---------|------|------------|-------|------|---------|------|------------|-------|------|---------|------|------------|------------|
| | | F1 | <u>om No</u> | <u>rth</u> | | | F | rom Ea | st | | | Fr | om So | uth | | | Fi | rom W | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis I | From 07 | 7:00 AN | 1 to 08 | :45 AM - | Peak 1 | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins a | t 07:30 A | M | | | | | | | | | | | | | | | |
| 07:30 AM | 25 | 69 | 10 | 1 | 105 | 9 | 61 | 19 | 1 | 90 | 21 | 61 | 9 | 1 | 92 | 7 | 80 | 28 | 0 | 115 | 402 |
| 07:45 AM | 50 | 105 | 6 | 0 | 161 | 8 | 81 | 31 | 0 | 120 | 33 | 50 | 9 | 0 | 92 | 5 | 82 | 36 | 0 | 123 | 496 |
| 08:00 AM | 21 | 73 | 5 | 0 | 99 | 14 | 72 | 22 | 0 | 108 | 39 | 80 | 9 | 0 | 128 | 6 | 102 | 30 | 0 | 138 | 473 |
| 08:15 AM | 18 | 59 | 9 | 0 | 86 | 7 | 62 | 23 | 0 | 92 | 19 | 52 | 5 | 1 | 77 | 3 | 79 | 23 | 0 | 105 | 360 |
| Total Volume | 114 | 306 | 30 | 1 | 451 | 38 | 276 | 95 | 1 | 410 | 112 | 243 | 32 | 2 | 389 | 21 | 343 | 117 | 0 | 481 | 1731 |
| % App. Total | 25.3 | 67.8 | 6.7 | 0.2 | | 9.3 | 67.3 | 23.2 | 0.2 | | 28.8 | 62.5 | 8.2 | 0.5 | | 4.4 | 71.3 | 24.3 | 0 | | |
| PHF | .570 | .729 | .750 | .250 | .700 | .679 | .852 | .766 | .250 | .854 | .718 | .759 | .889 | .500 | .760 | .750 | .841 | .813 | .000 | .871 | .872 |
| Cars & Peds | 111 | 302 | 29 | 1 | 443 | 38 | 272 | 91 | 1 | 402 | 109 | 238 | 32 | 2 | 381 | 20 | 339 | 117 | 0 | 476 | 1702 |
| % Cars & Peds | 97.4 | 98.7 | 96.7 | 100 | 98.2 | 100 | 98.6 | 95.8 | 100 | 98.0 | 97.3 | 97.9 | 100 | 100 | 97.9 | 95.2 | 98.8 | 100 | 0 | 99.0 | 98.3 |
| Trucks & Buses | 3 | 4 | 1 | 0 | 8 | 0 | 4 | 4 | 0 | 8 | 3 | 5 | 0 | 0 | 8 | 1 | 4 | 0 | 0 | 5 | 29 |
| % Trucks & Buses | 2.6 | 1.3 | 3.3 | 0 | 1.8 | 0 | 1.4 | 4.2 | 0 | 2.0 | 2.7 | 2.1 | 0 | 0 | 2.1 | 4.8 | 1.2 | 0 | 0 | 1.0 | 1.7 |
| Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |



N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | | | Grou | ips Printe | d- Cars & | z Peds - ' | Trucks & | & Buses - | Bikes by | Direction | on | | | | | |
|----------------------|-------|---------|-------|------|------------|-----------|------------|----------|-----------|----------|-----------|------|-------|----------|--------|------|------------|
| | | Dyer Av | venue | | - (| Cranston | Street | | | Dyer Av | /enue | | (| Cranston | Street | | |
| | | From N | lorth | | | From H | East | | | From S | outh | | | From V | Vest | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 03:00 PM | 34 | 67 | 11 | 1 | 12 | 85 | 18 | 0 | 24 | 74 | 1 | 0 | 7 | 61 | 30 | 0 | 425 |
| 03:15 PM | 32 | 61 | 9 | 0 | 11 | 73 | 22 | 0 | 21 | 76 | 0 | 0 | 6 | 67 | 38 | 2 | 418 |
| 03:30 PM | 32 | 69 | 12 | 0 | 11 | 73 | 16 | 0 | 19 | 77 | 2 | 1 | 4 | 62 | 39 | 0 | 417 |
| 03:45 PM | 31 | 79 | 15 | 0 | 13 | 68 | 17 | 0 | 25 | 59 | 4 | 0 | 6 | 71 | 31 | 3 | 422 |
| Total | 129 | 276 | 47 | 1 | 47 | 299 | 73 | 0 | 89 | 286 | 7 | 1 | 23 | 261 | 138 | 5 | 1682 |
| | | | | | | | | | | | | | | | | | |
| 04:00 PM | 39 | 63 | 11 | 0 | 12 | 85 | 27 | 0 | 21 | 89 | 4 | 2 | 5 | 64 | 35 | 0 | 457 |
| 04:15 PM | 25 | 65 | 10 | 0 | 12 | 69 | 20 | 1 | 26 | 78 | 4 | 0 | 6 | 51 | 37 | 1 | 405 |
| 04:30 PM | 27 | 71 | 16 | 0 | 11 | 96 | 23 | 0 | 20 | 75 | 8 | 0 | 0 | 55 | 39 | 0 | 441 |
| 04:45 PM | 30 | 80 | 9 | 0 | 13 | 77 | 21 | 0 | 23 | 65 | 2 | 0 | 7 | 61 | 39 | 0 | 427 |
| Total | 121 | 279 | 46 | 0 | 48 | 327 | 91 | 1 | 90 | 307 | 18 | 2 | 18 | 231 | 150 | 1 | 1730 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 26 | 52 | 12 | 1 | 12 | 72 | 18 | 0 | 26 | 71 | 3 | 0 | 5 | 50 | 30 | 0 | 378 |
| 05:15 PM | 32 | 56 | 15 | 0 | 17 | 81 | 23 | 0 | 23 | 73 | 7 | 0 | 2 | 43 | 25 | 0 | 397 |
| 05:30 PM | 30 | 50 | 13 | 0 | 6 | 54 | 26 | 0 | 10 | 55 | 7 | 1 | 2 | 51 | 22 | 0 | 327 |
| 05:45 PM | 17 | 63 | 14 | 0 | 11 | 48 | 25 | 0 | 26 | 54 | 2 | 0 | 7 | 47 | 20 | 0 | 334 |
| Total | 105 | 221 | 54 | 1 | 46 | 255 | 92 | 0 | 85 | 253 | 19 | 1 | 16 | 191 | 97 | 0 | 1436 |
| | | | | | | | | . 1 | | | | . 1 | | | | | |
| Grand Total | 355 | 776 | 147 | 2 | 141 | 881 | 256 | 1 | 264 | 846 | 44 | 4 | 57 | 683 | 385 | 6 | 4848 |
| Apprch % | 27.7 | 60.6 | 11.5 | 0.2 | 11 | 68.9 | 20 | 0.1 | 22.8 | 73.1 | 3.8 | 0.3 | 5 | 60.4 | 34 | 0.5 | |
| Total % | 7.3 | 16 | 3 | 0 | 2.9 | 18.2 | 5.3 | 0 | 5.4 | 17.5 | 0.9 | 0.1 | 1.2 | 14.1 | 7.9 | 0.1 | |
| Cars & Peds | 354 | 761 | 143 | 2 | 140 | 871 | 251 | 1 | 263 | 837 | 44 | 4 | 56 | 669 | 383 | 6 | 4785 |
| % Cars & Peds | 99.7 | 98.1 | 97.3 | 100 | 99.3 | 98.9 | 98 | 100 | 99.6 | 98.9 | 100 | 100 | 98.2 | 98 | 99.5 | 100 | 98.7 |
| Trucks & Buses | 1 | 14 | 4 | 0 | 1 | 10 | 5 | 0 | 1 | 9 | 0 | 0 | 1 | 13 | 2 | 0 | 61 |
| % Trucks & Buses | 0.3 | 1.8 | 2.7 | 0 | 0.7 | 1.1 | 2 | 0 | 0.4 | 1.1 | 0 | 0 | 1.8 | 1.9 | 0.5 | 0 | 1.3 |
| Bikes by Direction | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| % Bikes by Direction | 0 | 0.1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.1 | 0 | 0 | 0 |

| | | 2 | ver Ave | | | | | iston St | | | | 2 | er Ave | | | | | ston St | | | |
|----------------------|--------|---------|---------|---------|------------|-------|------|----------|------|------------|-------|------|--------|------|------------|-------|------|---------|------|------------|------------|
| | | Fi | rom No | rth | | | F | rom Ea | st | | | | om Sou | ith | | | F | rom We | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | | | | | | | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins a | t 04:00 P | М | | | | | | | | | | | | | | | |
| 04:00 PM | 39 | 63 | 11 | 0 | 113 | 12 | 85 | 27 | 0 | 124 | 21 | 89 | 4 | 2 | 116 | 5 | 64 | 35 | 0 | 104 | 457 |
| 04:15 PM | 25 | 65 | 10 | 0 | 100 | 12 | 69 | 20 | 1 | 102 | 26 | 78 | 4 | 0 | 108 | 6 | 51 | 37 | 1 | 95 | 405 |
| 04:30 PM | 27 | 71 | 16 | 0 | 114 | 11 | 96 | 23 | 0 | 130 | 20 | 75 | 8 | 0 | 103 | 0 | 55 | 39 | 0 | 94 | 441 |
| 04:45 PM | 30 | 80 | 9 | 0 | 119 | 13 | 77 | 21 | 0 | 111 | 23 | 65 | 2 | 0 | 90 | 7 | 61 | 39 | 0 | 107 | 427 |
| Total Volume | 121 | 279 | 46 | 0 | 446 | 48 | 327 | 91 | 1 | 467 | 90 | 307 | 18 | 2 | 417 | 18 | 231 | 150 | 1 | 400 | 1730 |
| % App. Total | 27.1 | 62.6 | 10.3 | 0 | | 10.3 | 70 | 19.5 | 0.2 | | 21.6 | 73.6 | 4.3 | 0.5 | | 4.5 | 57.8 | 37.5 | 0.2 | | |
| PHF | .776 | .872 | .719 | .000 | .937 | .923 | .852 | .843 | .250 | .898 | .865 | .862 | .563 | .250 | .899 | .643 | .902 | .962 | .250 | .935 | .946 |
| Cars & Peds | 121 | 277 | 44 | 0 | 442 | 47 | 323 | 90 | 1 | 461 | 90 | 304 | 18 | 2 | 414 | 18 | 227 | 148 | 1 | 394 | 1711 |
| % Cars & Peds | 100 | 99.3 | 95.7 | 0 | 99.1 | 97.9 | 98.8 | 98.9 | 100 | 98.7 | 100 | 99.0 | 100 | 100 | 99.3 | 100 | 98.3 | 98.7 | 100 | 98.5 | 98.9 |
| Trucks & Buses | 0 | 2 | 2 | 0 | 4 | 1 | 4 | 1 | 0 | 6 | 0 | 3 | 0 | 0 | 3 | 0 | 4 | 2 | 0 | 6 | 19 |
| % Trucks & Buses | 0 | 0.7 | 4.3 | 0 | 0.9 | 2.1 | 1.2 | 1.1 | 0 | 1.3 | 0 | 1.0 | 0 | 0 | 0.7 | 0 | 1.7 | 1.3 | 0 | 1.5 | 1.1 |
| Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | | | | | G | roups Pr | inted- Ca | ars & Pec | ls | | | | | | | |
|-------------|-------|--------|-------|------|-------|----------|----------|-----------|-----------|---------|-------|------|-------|----------|--------|------|------------|
| | | Dyer A | venue | | (| Cranston | Street | | | Dyer Av | venue | | (| Cranston | Street | | |
| | | From 1 | | | | From 1 | East | | | From S | outh | | | From | West | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 03:00 PM | 34 | 66 | 11 | 1 | 12 | 84 | 18 | 0 | 24 | 73 | 1 | 0 | 6 | 60 | 30 | 0 | 420 |
| 03:15 PM | 32 | 60 | 9 | 0 | 11 | 72 | 20 | 0 | 21 | 76 | 0 | 0 | 6 | 65 | 38 | 2 | 412 |
| 03:30 PM | 32 | 67 | 11 | 0 | 11 | 73 | 15 | 0 | 19 | 75 | 2 | 1 | 4 | 62 | 39 | 0 | 411 |
| 03:45 PM | 31 | 76 | 14 | 0 | 13 | 65 | 17 | 0 | 25 | 59 | 4 | 0 | 6 | 70 | 31 | 3 | 414 |
| Total | 129 | 269 | 45 | 1 | 47 | 294 | 70 | 0 | 89 | 283 | 7 | 1 | 22 | 257 | 138 | 5 | 1657 |
| | | | | | | | | | | | | | | | | | |
| 04:00 PM | 39 | 63 | 9 | 0 | 12 | 85 | 27 | 0 | 21 | 89 | 4 | 2 | 5 | 61 | 34 | 0 | 451 |
| 04:15 PM | 25 | 64 | 10 | 0 | 11 | 68 | 19 | 1 | 26 | 77 | 4 | 0 | 6 | 51 | 37 | 1 | 400 |
| 04:30 PM | 27 | 70 | 16 | 0 | 11 | 94 | 23 | 0 | 20 | 75 | 8 | 0 | 0 | 54 | 38 | 0 | 436 |
| 04:45 PM | 30 | 80 | 9 | 0 | 13 | 76 | 21 | 0 | 23 | 63 | 2 | 0 | 7 | 61 | 39 | 0 | 424 |
| Total | 121 | 277 | 44 | 0 | 47 | 323 | 90 | 1 | 90 | 304 | 18 | 2 | 18 | 227 | 148 | 1 | 1711 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 25 | 51 | 12 | 1 | 12 | 72 | 18 | 0 | 26 | 71 | 3 | 0 | 5 | 47 | 30 | 0 | 373 |
| 05:15 PM | 32 | 54 | 15 | 0 | 17 | 81 | 22 | 0 | 22 | 71 | 7 | 0 | 2 | 43 | 25 | 0 | 391 |
| 05:30 PM | 30 | 48 | 13 | 0 | 6 | 53 | 26 | 0 | 10 | 55 | 7 | 1 | 2 | 50 | 22 | 0 | 323 |
| 05:45 PM | 17 | 62 | 14 | 0 | 11 | 48 | 25 | 0 | 26 | 53 | 2 | 0 | 7 | 45 | 20 | 0 | 330 |
| Total | 104 | 215 | 54 | 1 | 46 | 254 | 91 | 0 | 84 | 250 | 19 | 1 | 16 | 185 | 97 | 0 | 1417 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 354 | 761 | 143 | 2 | 140 | 871 | 251 | 1 | 263 | 837 | 44 | 4 | 56 | 669 | 383 | 6 | 4785 |
| Apprch % | 28.1 | 60.4 | 11.3 | 0.2 | 11.1 | 69 | 19.9 | 0.1 | 22.9 | 72.9 | 3.8 | 0.3 | 5 | 60.1 | 34.4 | 0.5 | |
| Total % | 7.4 | 15.9 | 3 | 0 | 2.9 | 18.2 | 5.2 | 0 | 5.5 | 17.5 | 0.9 | 0.1 | 1.2 | 14 | 8 | 0.1 | |

| | | Dy | er Ave | nue | | | Cra | iston S | treet | | | Dy | ver Ave | nue | | | Crai | iston St | treet | |] |
|---------------|----------|---------|---------|----------|------------|--------|------|---------|-------|------------|-------|------|---------|------|------------|-------|------|----------|-------|------------|------------|
| | | Fı | rom No | rth | | | F | rom Ea | ıst | | | Fr | om Sou | ıth | | | F | rom We | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis I | From 03 | 3:00 PM | 1 to 05: | 45 PM - | Peak 1 | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins a | t 04:00 P | Μ | | | | | | | | | | | | | | | |
| 04:00 PM | 39 | 63 | 9 | 0 | 111 | 12 | 85 | 27 | 0 | 124 | 21 | 89 | 4 | 2 | 116 | 5 | 61 | 34 | 0 | 100 | 451 |
| 04:15 PM | 25 | 64 | 10 | 0 | 99 | 11 | 68 | 19 | 1 | 99 | 26 | 77 | 4 | 0 | 107 | 6 | 51 | 37 | 1 | 95 | 400 |
| 04:30 PM | 27 | 70 | 16 | 0 | 113 | 11 | 94 | 23 | 0 | 128 | 20 | 75 | 8 | 0 | 103 | 0 | 54 | 38 | 0 | 92 | 436 |
| 04:45 PM | 30 | 80 | 9 | 0 | 119 | 13 | 76 | 21 | 0 | 110 | 23 | 63 | 2 | 0 | 88 | 7 | 61 | 39 | 0 | 107 | 424 |
| Total Volume | 121 | 277 | 44 | 0 | 442 | 47 | 323 | 90 | 1 | 461 | 90 | 304 | 18 | 2 | 414 | 18 | 227 | 148 | 1 | 394 | 1711 |
| % App. Total | 27.4 | 62.7 | 10 | 0 | | 10.2 | 70.1 | 19.5 | 0.2 | | 21.7 | 73.4 | 4.3 | 0.5 | | 4.6 | 57.6 | 37.6 | 0.3 | | |
| PHF | .776 | .866 | .688 | .000 | .929 | .904 | .859 | .833 | .250 | .900 | .865 | .854 | .563 | .250 | .892 | .643 | .930 | .949 | .250 | .921 | .948 |

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | | | | | Gro | ups Prin | ted- Tru | cks & Bu | ises | | | | | | | |
|-------------|-------|--------|-------|------|-------|----------|----------|----------|----------|--------|-------|------|-------|----------|--------|------|------------|
| | | Dyer A | venue | | (| Cranston | Street | | | Dyer A | venue | | (| Cranston | Street | | |
| | | From 1 | North | | | From 1 | East | | | From S | outh | | | From | West | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 03:00 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 5 |
| 03:15 PM | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 |
| 03:30 PM | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 03:45 PM | 0 | 3 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 8 |
| Total | 0 | 6 | 2 | 0 | 0 | 5 | 3 | 0 | 0 | 3 | 0 | 0 | 1 | 3 | 0 | 0 | 23 |
| | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 6 |
| 04:15 PM | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 04:30 PM | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 5 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Total | 0 | 2 | 2 | 0 | 1 | 4 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 4 | 2 | 0 | 19 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 5 |
| 05:15 PM | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 05:30 PM | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 |
| 05:45 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 4 |
| Total | 1 | 6 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 3 | 0 | 0 | 0 | 6 | 0 | 0 | 19 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 1 | 14 | 4 | 0 | 1 | 10 | 5 | 0 | 1 | 9 | 0 | 0 | 1 | 13 | 2 | 0 | 61 |
| Apprch % | 5.3 | 73.7 | 21.1 | 0 | 6.2 | 62.5 | 31.2 | 0 | 10 | 90 | 0 | 0 | 6.2 | 81.2 | 12.5 | 0 | |
| Total % | 1.6 | 23 | 6.6 | 0 | 1.6 | 16.4 | 8.2 | 0 | 1.6 | 14.8 | 0 | 0 | 1.6 | 21.3 | 3.3 | 0 | |

| | | Dy | ver Ave | nue | | | Crai | ston St | reet | | | Dy | er Ave | nue | | | Crar | ston S | treet | |] |
|---------------|----------|---------|---------|----------|------------|--------|------|---------|------|------------|-------|------|--------|------|------------|-------|------|--------|-------|------------|------------|
| | | Fi | rom No | orth | | | F | rom Ea | st | | | Fr | om Sou | ıth | | | F | rom We | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis F | From 03 | 3:00 PN | 4 to 05: | 45 PM - | Peak 1 | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins a | t 03:30 P | Μ | | | | | | | | | | | | | | | |
| 03:30 PM | 0 | 2 | 1 | 0 | 3 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 6 |
| 03:45 PM | 0 | 3 | 1 | 0 | 4 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 8 |
| 04:00 PM | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 4 | 6 |
| 04:15 PM | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 3 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 |
| Total Volume | 0 | 6 | 4 | 0 | 10 | 1 | 4 | 2 | 0 | 7 | 0 | 3 | 0 | 0 | 3 | 0 | 4 | 1 | 0 | 5 | 25 |
| % App. Total | 0 | 60 | 40 | 0 | | 14.3 | 57.1 | 28.6 | 0 | | 0 | 100 | 0 | 0 | | 0 | 80 | 20 | 0 | | |
| PHF | .000 | .500 | .500 | .000 | .625 | .250 | .333 | .500 | .000 | .583 | .000 | .375 | .000 | .000 | .375 | .000 | .333 | .250 | .000 | .313 | .781 |

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| File Name | : 05662AA |
|------------|-------------|
| Site Code | : 9575 |
| Start Date | : 1/10/2023 |
| Page No | : 1 |

| | | | | | | Grou | ps Printe | ed- Bike | s by Dire | ction | | | | | | | |
|-------------|-------|---------|-------|------|-------|----------|-----------|----------|-----------|--------|-------|------|-------|----------|--------|------|------------|
| | | Dyer Av | venue | | | Cranston | Street | | | Dyer A | venue | | (| Cranston | Street | | |
| | | From N | North | | | From 1 | East | | | From S | outh | | | From | West | | |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| 03:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| 03:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| Apprch % | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | |
| Total % | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 0 | |

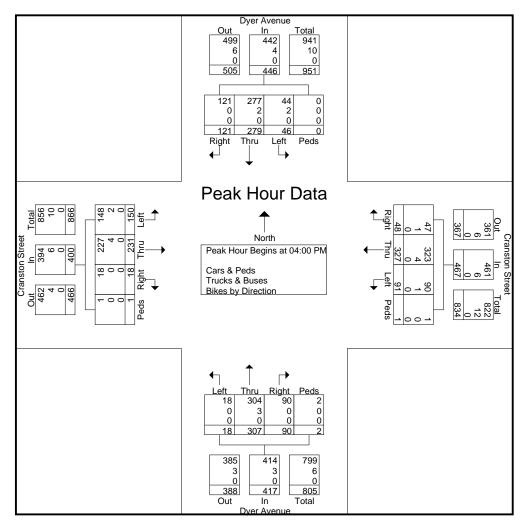
| | | - | ver Ave | | | | | ston S | | | | 2 | er Ave | | | | | nston S | | | |
|---------------|----------|---------|---------|----------|------------|--------|------|--------|------|------------|-------|------|--------|------|------------|-------|------|---------|------|------------|------------|
| | | Fi | rom No | rth | | | F | rom Ea | st | | | Fr | om Sou | ıth | | | F | rom We | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis F | From 03 | 3:00 PN | 1 to 05: | 45 PM - | Peak 1 | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins a | t 03:00 P | М | | | | | | | | | | | | | | | |
| 03:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| 03:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| % App. Total | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .000 | .250 | .250 |

Transportation Data Corporation

Mario Perone, mperone1@verizon.net tel (781) 587-0086 cell (781) 439-4999

N/S: Dyer Avenue E/W: Cranston Street City, State: Cranston, RI Client: VAI/D. Roach

| | | Dy | ver Ave | nue | | | Crar | nston St | treet | | | Dy | ver Ave | nue | | | Crai | nston S | treet | | |
|----------------------|----------|---------|---------|----------|------------|--------|------|----------|-------|------------|-------|------|---------|------|------------|-------|------|---------|-------|------------|------------|
| | | Fi | om No | rth | | | F | rom Ea | ıst | | | Fr | om So | uth | | | F | rom W | est | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour An | alysis I | From 03 | 3:00 PM | 1 to 05: | 45 PM - | Peak 1 | of 1 | | | | | | | | | | | | | | |
| Peak Hour for | Entire | Interse | ction B | egins at | t 04:00 P | М | | | | | | | | | | | | | | | |
| 04:00 PM | 39 | 63 | 11 | 0 | 113 | 12 | 85 | 27 | 0 | 124 | 21 | 89 | 4 | 2 | 116 | 5 | 64 | 35 | 0 | 104 | 457 |
| 04:15 PM | 25 | 65 | 10 | 0 | 100 | 12 | 69 | 20 | 1 | 102 | 26 | 78 | 4 | 0 | 108 | 6 | 51 | 37 | 1 | 95 | 405 |
| 04:30 PM | 27 | 71 | 16 | 0 | 114 | 11 | 96 | 23 | 0 | 130 | 20 | 75 | 8 | 0 | 103 | 0 | 55 | 39 | 0 | 94 | 441 |
| 04:45 PM | 30 | 80 | 9 | 0 | 119 | 13 | 77 | 21 | 0 | 111 | 23 | 65 | 2 | 0 | 90 | 7 | 61 | 39 | 0 | 107 | 427 |
| Total Volume | 121 | 279 | 46 | 0 | 446 | 48 | 327 | 91 | 1 | 467 | 90 | 307 | 18 | 2 | 417 | 18 | 231 | 150 | 1 | 400 | 1730 |
| % App. Total | 27.1 | 62.6 | 10.3 | 0 | | 10.3 | 70 | 19.5 | 0.2 | | 21.6 | 73.6 | 4.3 | 0.5 | | 4.5 | 57.8 | 37.5 | 0.2 | | |
| PHF | .776 | .872 | .719 | .000 | .937 | .923 | .852 | .843 | .250 | .898 | .865 | .862 | .563 | .250 | .899 | .643 | .902 | .962 | .250 | .935 | .946 |
| Cars & Peds | 121 | 277 | 44 | 0 | 442 | 47 | 323 | 90 | 1 | 461 | 90 | 304 | 18 | 2 | 414 | 18 | 227 | 148 | 1 | 394 | 1711 |
| % Cars & Peds | 100 | 99.3 | 95.7 | 0 | 99.1 | 97.9 | 98.8 | 98.9 | 100 | 98.7 | 100 | 99.0 | 100 | 100 | 99.3 | 100 | 98.3 | 98.7 | 100 | 98.5 | 98.9 |
| Trucks & Buses | 0 | 2 | 2 | 0 | 4 | 1 | 4 | 1 | 0 | 6 | 0 | 3 | 0 | 0 | 3 | 0 | 4 | 2 | 0 | 6 | 19 |
| % Trucks & Buses | 0 | 0.7 | 4.3 | 0 | 0.9 | 2.1 | 1.2 | 1.1 | 0 | 1.3 | 0 | 1.0 | 0 | 0 | 0.7 | 0 | 1.7 | 1.3 | 0 | 1.5 | 1.1 |
| Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % Bikes by Direction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |



Cranston, Rhode Island

APPENDIX B – Traffic Crash Data

January 2018 through December 2019 & January 2022 through December 2022

Cranston Street at Dyer Avenue Cranston Street

Dyer Avenue



Crash Data Summary

| | | Year | | Total | Average |
|--------------------------------|------|------|------|-------|----------|
| | 2018 | 2019 | 2022 | TOtal | per Year |
| Intersections | | | | | |
| Cranston Street at Dyer Avenue | 13 | 15 | 9 | 37 | 12 |
| Roadways | | | | | |
| Cranston Street | 3 | 0 | 1 | 4 | 1 |
| Dyer Avenue | 3 | 2 | 1 | 6 | 2 |
| Total | 19 | 17 | 11 | 47 | 15 |



| | | 2018 | 2019 | 2022 | Total | Percent |
|----------|-------------------------------|------|------|------|-------|---------|
| | | | 1 | | | |
| Collisio | | | | | | |
| | Rear End | 4 | 5 | 1 | 10 | 27% |
| | Angle | 5 | 4 | 6 | 15 | 41% |
| | Head-On | 2 | 1 | 0 | 3 | 8% |
| | Pedestrian | 0 | 0 | 0 | 0 | 0% |
| | Sideswipe, Same Direction | 2 | 4 | 2 | 8 | 22% |
| | Sideswipe, Opposite Direction | 0 | 0 | 0 | 0 | 0% |
| | Rear-to-Side | 0 | 0 | 0 | 0 | 0% |
| | Rear-to-Rear | 0 | 0 | 0 | 0 | 0% |
| | Collision with Object | 0 | 1 | 0 | 1 | 3% |
| | Collision with Deer | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| | | | | | | |
| Crash S | everity | | | | | |
| | Property | 0 | 0 | 0 | 0 | 0% |
| | Injury | 0 | 0 | 0 | 0 | 0% |
| | Fatal | 0 | 0 | 0 | 0 | 0% |
| | | | | | | |
| Light Co | ondition | | | | | |
| | Daylight | 12 | 10 | 6 | 28 | 76% |
| | Dawn | 0 | 0 | 1 | 1 | 3% |
| | Dusk | 0 | 0 | 0 | 0 | 0% |
| | Dark - Lighted | 1 | 5 | 2 | 8 | 22% |
| | Dark - Not Lighted | 0 | 0 | 0 | 0 | 0% |
| | Dark - Unknown Lighting | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| | | | | | | |
| Road C | ondition | | | - | | |
| | Dry | 12 | 13 | 8 | 33 | 89% |
| | Wet | 1 | 2 | 1 | 4 | 11% |
| | Snow | 0 | 0 | 0 | 0 | 0% |
| | Slush | 0 | 0 | 0 | 0 | 0% |
| | Ice/Frost | 0 | 0 | 0 | 0 | 0% |
| | Water | 0 | 0 | 0 | 0 | 0% |
| | Sand | 0 | 0 | 0 | 0 | 0% |
| | Mud, Dirt, Gravel | 0 | 0 | 0 | 0 | 0% |
| | Oil | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| | - | | | | | |
| Hour of | | | | | - | 4.101 |
| | 6:00 AM - 9:00 AM | 1 | 2 | 1 | 4 | 11% |
| | 9:00 AM - 3:00 PM | 7 | 5 | 2 | 14 | 38% |
| | 3:00 PM - 6:00 PM | 3 | 3 | 4 | 10 | 27% |
| | 6:00 PM - 6:00 AM | 2 | 5 | 2 | 9 | 24% |
| | | | | | | |
| | Total Crashes: | 13 | 15 | 9 | 37 | |

Cranston Street at Dyer Avenue



| | | 2018 | 2019 | 2022 | Total | Percent |
|---------|-------------------------------|------|------|------|--------|---------|
| | | | | | | |
| Collisi | ion Type | | | | | |
| | Rear End | 1 | 0 | 0 | 1 | 25% |
| | Angle | 0 | 0 | 1 | 1 | 25% |
| | Head-On | 0 | 0 | 0 | 0 | 0% |
| | Pedestrian | 0 | 0 | 0 | 0 | 0% |
| | Sideswipe, Same Direction | 1 | 0 | 0 | 1 | 25% |
| | Sideswipe, Opposite Direction | 0 | 0 | 0 | 0 | 0% |
| | Rear-to-Side | 0 | 0 | 0 | 0 | 0% |
| | Rear-to-Rear | 0 | 0 | 0 | 0 | 0% |
| | Collision with Object | 1 | 0 | 0 | 1 | 25% |
| | Collision with Deer | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| | | | | | | |
| Crash | Severity | | | | | |
| | Property | 0 | 0 | 0 | 0 | 0% |
| | Injury | 0 | 0 | 0 | 0 | 0% |
| | Fatal | 0 | 0 | 0 | 0 | 0% |
| | | | | | | |
| Light | Condition | | - | | | |
| | Daylight | 3 | 0 | 1 | 4 | 100% |
| | Dawn | 0 | 0 | 0 | 0 | 0% |
| | Dusk | 0 | 0 | 0 | 0 | 0% |
| | Dark - Lighted | 0 | 0 | 0 | 0 | 0% |
| | Dark - Not Lighted | 0 | 0 | 0 | 0 | 0% |
| | Dark - Unknown Lighting | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| Deed | | | | | | |
| коаа | Condition | 2 | 0 | 1 | 3 | 75% |
| | Dry | | - | | 3 1 | |
| | Wet | 1 | 0 | 0 | _ | 25% |
| | Snow | 0 | 0 | 0 | 0 | 0% |
| | Slush | 0 | 0 | 0 | 0 | 0% |
| | Ice/Frost | 0 | 0 | 0 | 0 | 0% |
| | Water | 0 | 0 | 0 | 0 | 0% |
| | Sand | 0 | 0 | 0 | 0 | 0% |
| | Mud, Dirt, Gravel | 0 | 0 | 0 | 0 | 0% |
| | Oil | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| Hour | of Day | | | | | |
| nour | 6:00 AM - 9:00 AM | 0 | 0 | 0 | 0 | 0% |
| | 9:00 AM - 3:00 PM | 1 | 0 | 1 | 2 | 50% |
| | 3:00 PM - 6:00 PM | 2 | 0 | 0 | 2 | 50% |
| | 6:00 PM - 6:00 PM | 0 | 0 | 0 | 0 | 0% |
| | 0.00 FWI - 0.00 AWI | U | U | 0 | U | 070 |
| | Total Crashes: | 3 | 0 | 1 | 4 | - |

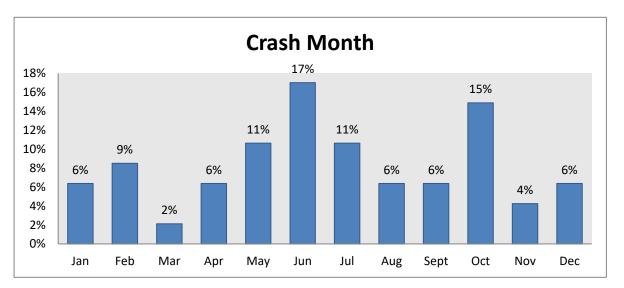
Cranston Street



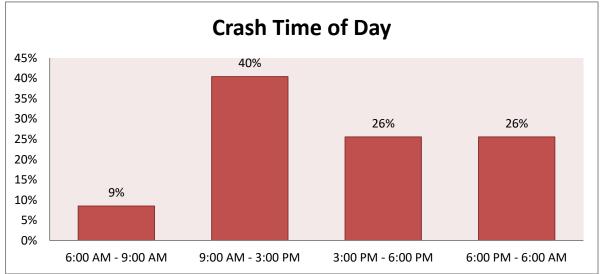
| Dyer | Avenue |
|------|--------|
| | |

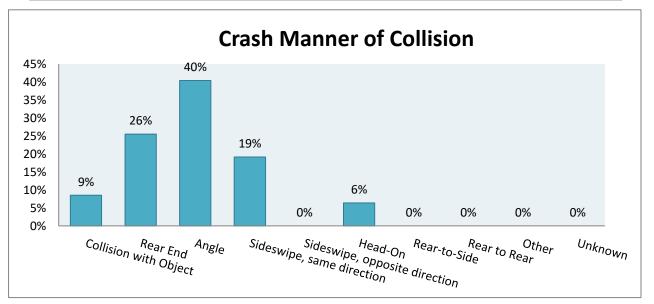
| | | 2018 | 2019 | 2022 | Total | Percent |
|--------|-------------------------------|------|------|------|-------|---------|
| Call!- | ion Tuno | | | | | |
| Collis | ion Type Rear End | 0 | 1 | 0 | 1 | 17% |
| | | 3 | 0 | 0 | 3 | 50% |
| | Angle Head-On | 0 | 0 | 0 | 0 | 0% |
| | | | - | - | | |
| | Pedestrian | 0 | 0 | 0 | 0 | 0% |
| | Sideswipe, Same Direction | 0 | 0 | 0 | 0 | 0% |
| | Sideswipe, Opposite Direction | 0 | 0 | 0 | 0 | 0% |
| | Rear-to-Side | 0 | 0 | 0 | 0 | 0% |
| | Rear-to-Rear | 0 | 0 | 0 | 0 | 0% |
| | Collision with Object | 0 | 1 | 1 | 2 | 33% |
| | Collision with Deer | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| Crash | Severity | | | | | |
| | Property | 0 | 0 | 0 | 0 | 0% |
| | Injury | 0 | 0 | 0 | 0 | 0% |
| | Fatal | 0 | 0 | 0 | 0 | 0% |
| | | | | | | |
| ight | Condition | | | | | |
| | Daylight | 2 | 1 | 0 | 3 | 50% |
| | Dawn | 0 | 0 | 0 | 0 | 0% |
| | Dusk | 0 | 0 | 0 | 0 | 0% |
| | Dark - Lighted | 1 | 1 | 1 | 3 | 50% |
| | Dark - Not Lighted | 0 | 0 | 0 | 0 | 0% |
| | Dark - Unknown Lighting | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| Pood | Condition | | | | | |
| Noau | | 3 | 2 | 0 | 5 | 83% |
| | Dry Wet | 0 | 0 | 1 | 5 | 17% |
| | Snow | 0 | 0 | 0 | 0 | 0% |
| | Slush | 0 | 0 | 0 | 0 | 0% |
| | Ice/Frost | 0 | 0 | 0 | 0 | 0% |
| | | 0 | 0 | 0 | 0 | 0% |
| | Water Sand | 0 | 0 | 0 | 0 | 0% |
| | Mud, Dirt, Gravel | 0 | 0 | 0 | 0 | 0% |
| | Oil | 0 | 0 | 0 | 0 | 0% |
| | Other | 0 | 0 | 0 | 0 | 0% |
| | Unknown | 0 | 0 | 0 | 0 | 0% |
| | GHKHOWH | U | U | U | U | 0% |
| lour | of Day | | | | | |
| | 6:00 AM - 9:00 AM | 0 | 0 | 0 | 0 | 0% |
| | 9:00 AM - 3:00 PM | 2 | 1 | 0 | 3 | 50% |
| | 3:00 PM - 6:00 PM | 0 | 0 | 0 | 0 | 0% |
| | 6:00 PM - 6:00 AM | 1 | 1 | 1 | 3 | 50% |
| | | | | | | |
| | Total Crashes: | 3 | 2 | 1 | 6 | |



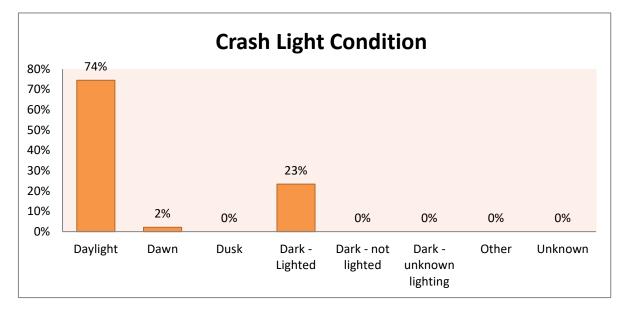


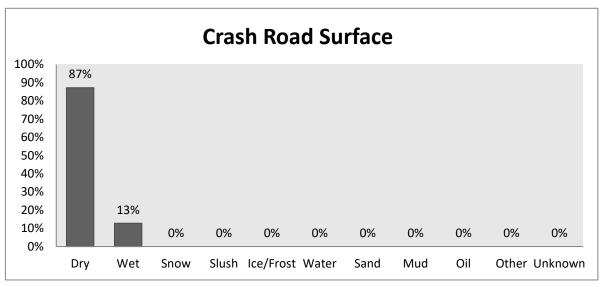
Crash Data Summary Charts



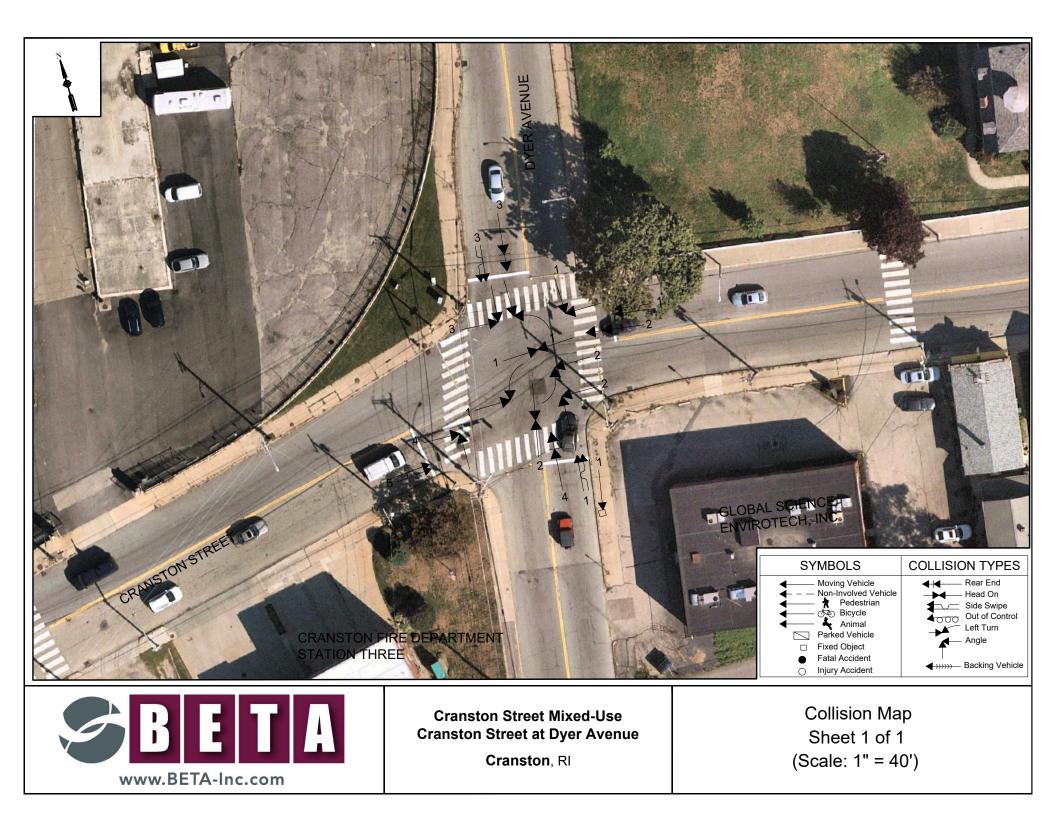












APPENDIX C – Trip Generation

ITE Trip Generation Summary

Site Trip Distribution

ITE Land Use Code

ITE Land Use Code 220 – Multifamily Housing (Low-Rise)

ITE Land Use Code 931 – Fine Dining Restaurant



С

ITE Trip Generation Summary



Trip Generation Summary

Summary;

| | Description | Enter | <u>Exit</u> | <u>Total</u> |
|-----------------------|-----------------------------------|-----------|-------------|--------------|
| Weekday AM Peak Hour | | | | |
| ITE Land Use Code 220 | Residential - Multifamily Housing | 17 | 54 | 71 |
| ITE Land Use Code 931 | Services - Fine Dining Restaurant | <u>0</u> | <u>0</u> | <u>0</u> |
| | TOTAL | 17 | 54 | 71 |
| Weekday PM Peak Hour | | | | |
| ITE Land Use Code 220 | Residential - Multifamily Housing | 56 | 32 | 88 |
| ITE Land Use Code 931 | Services - Fine Dining Restaurant | <u>19</u> | <u>8</u> | <u>27</u> |
| | TOTAL | 75 | 40 | 115 |



Calculations;

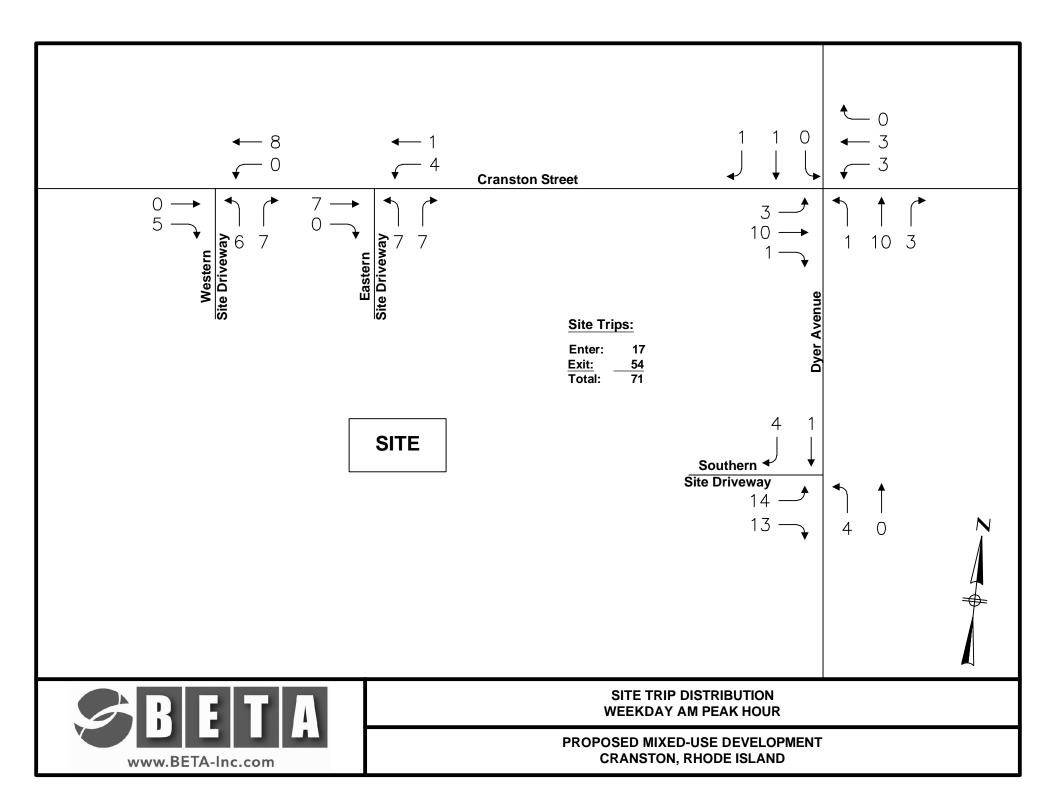
| ITE Land Use Code 220 | Residential - Multifamily Housing (Low Rise) | (156 | Units) |
|-----------------------|--|---|---------|
| Independent Var | iable (X) = Dwelling Units | X = 156 | |
| AM Peak | Directional Distribution: | 24% Entering 76% Exiting | |
| | T = 0.31 x (X) + T = 0.31 x 156 + T = 71 | 22.85 Enter: 17 22.85 <u>Exit: 54</u> Total: 71 | |
| PM Peak | Directional Distribution: | 63% Entering 37% Exiting | |
| | $T = 0.43 \times (X) + T = 0.43 \times 156 + T = 88$ | 20.55 Enter: 56 20.55 <u>Exit: 32</u> Total: 88 | |
| ITE Land Use Code 931 | Services - Fine Dining Restaurant 931 | 96 | 6 Seats |
| Independent Var | iable (X) = Seats | X = 96 | |
| PM Peak | Directional Distribution: | 67% Entering 33% Exiting | |
| | $T = 0.28 \times (X) T = 0.28 \times 96 T = 27$ | Enter: 19 Exit: 8 Total: 27 | |

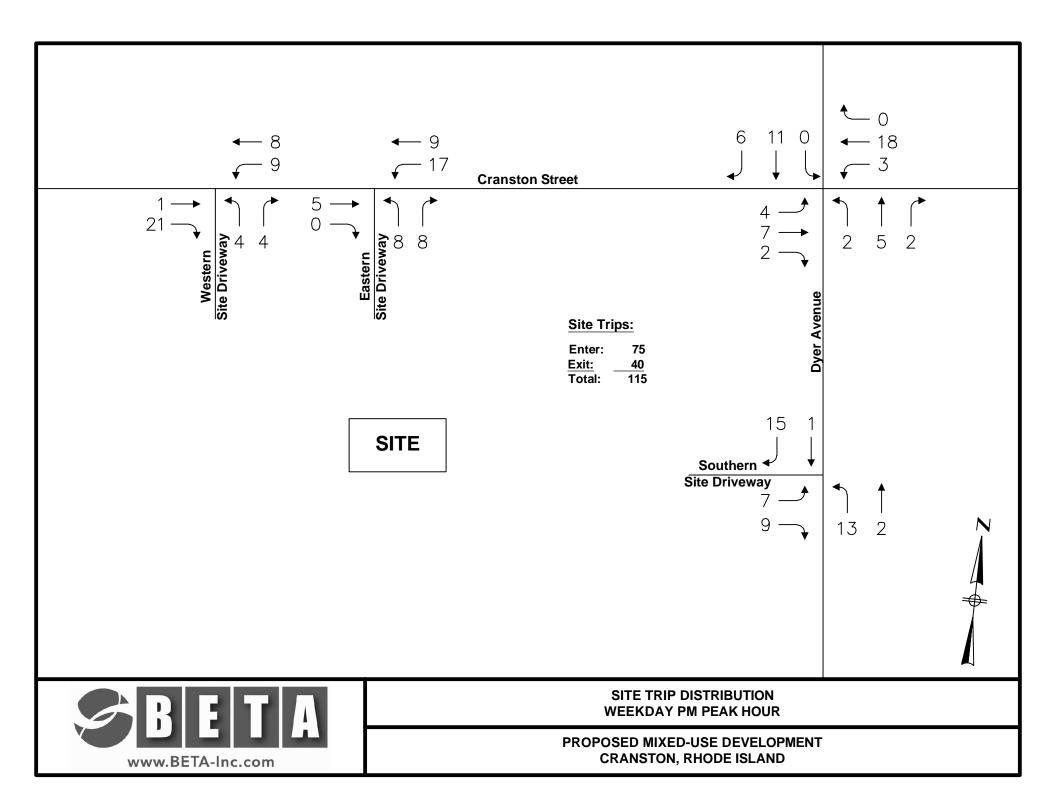


С

Site Trip Distribution







С

ITE Land Use Code

ITE Land Use Code 220 – Multifamily Housing (Low-Rise) ITE Land Use Code 931 – Fine Dining Restaurant



ITE Land Use Code 220 – Multifamily Housing (Low-Rise)



Land Use: 220 Multifamily Housing (Low-Rise)

Description

Low-rise multifamily housing includes apartments, townhouses, and condominiums located within the same building with at least three other dwelling units and that have two or three floors (levels). Various configurations fit this description, including walkup apartment, mansion apartment, and stacked townhouse.

- A walkup apartment typically is two or three floors in height with dwelling units that are accessed by a single or multiple entrances with stairways and hallways.
- A mansion apartment is a single structure that contains several apartments within what appears to be a single-family dwelling unit.
- A fourplex is a single two-story structure with two matching dwelling units on the ground and second floors. Access to the individual units is typically internal to the structure and provided through a central entry and stairway.
- A stacked townhouse is designed to match the external appearance of a townhouse. But, unlike a townhouse dwelling unit that only shares walls with an adjoining unit, the stacked townhouse units share both floors and walls. Access to the individual units is typically internal to the structure and provided through a central entry and stairway.

Multifamily housing (mid-rise) (Land Use 221), multifamily housing (high-rise) (Land Use 222), affordable housing (Land Use 223), and off-campus student apartment (low-rise) (Land Use 225) are related land uses.

Land Use Subcategory

Data are presented for two subcategories for this land use: (1) not close to rail transit and (2) close to rail transit. A site is considered close to rail transit if the walking distance between the residential site entrance and the closest rail transit station entrance is ½ mile or less.

Additional Data

For the three sites for which both the number of residents and the number of occupied dwelling units were available, there were an average of 2.72 residents per occupied dwelling unit.

For the two sites for which the numbers of both total dwelling units and occupied dwelling units were available, an average of 96.2 percent of the total dwelling units were occupied.

The technical appendices provide supporting information on time-of-day distributions for this land use. The appendices can be accessed through either the ITETripGen web app or the trip



generation resource page on the ITE website (https://www.ite.org/technical-resources/topics/tripand-parking-generation/).

For the three sites for which data were provided for both occupied dwelling units and residents, there was an average of 2.72 residents per occupied dwelling unit.

It is expected that the number of bedrooms and number of residents are likely correlated to the trips generated by a residential site. To assist in future analysis, trip generation studies of all multifamily housing should attempt to obtain information on occupancy rate and on the mix of residential unit sizes (i.e., number of units by number of bedrooms at the site complex).

The sites were surveyed in the 1980s, the 1990s, the 2000s, the 2010s, and the 2020s in British Columbia (CAN), California, Delaware, Florida, Georgia, Illinois, Indiana, Maine, Maryland, Massachusetts, Minnesota, New Jersey, Ontario (CAN), Oregon, Pennsylvania, South Carolina, South Dakota, Tennessee, Texas, Utah, and Washington.

Source Numbers

188, 204, 237, 300, 305, 306, 320, 321, 357, 390, 412, 525, 530, 579, 583, 638, 864, 866, 896, 901, 903, 904, 936, 939, 944, 946, 947, 948, 963, 964, 966, 967, 1012, 1013, 1014, 1036, 1047, 1056, 1071, 1076



Multifamily Housing (Low-Rise) Not Close to Rail Transit (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

Number of Studies: 49

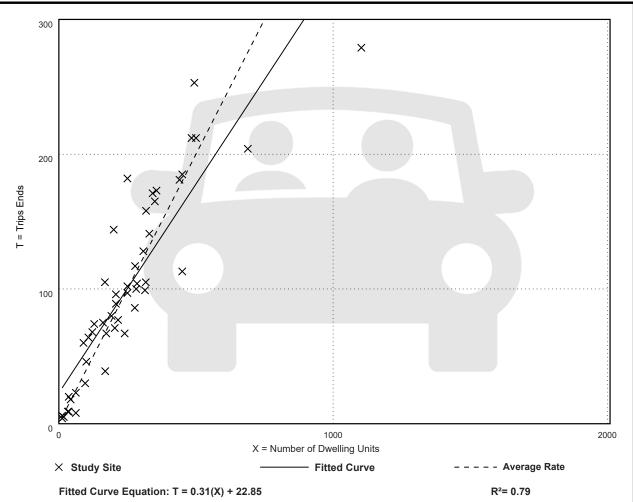
Avg. Num. of Dwelling Units: 249

Directional Distribution: 24% entering, 76% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.40 | 0.13 - 0.73 | 0.12 |

Data Plot and Equation



Multifamily Housing (Low-Rise) Not Close to Rail Transit (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 59

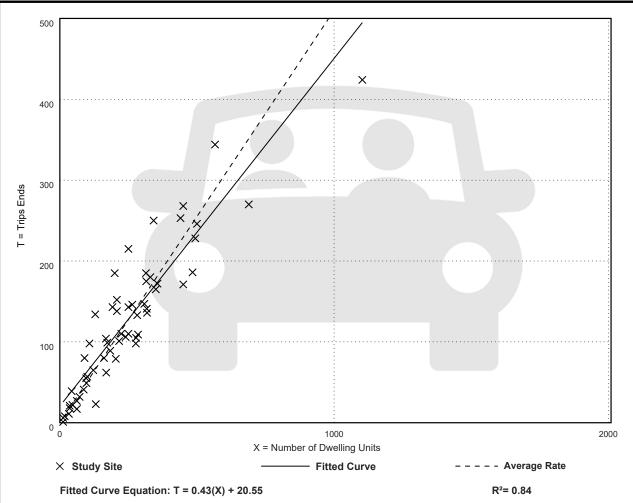
Avg. Num. of Dwelling Units: 241

Directional Distribution: 63% entering, 37% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.51 | 0.08 - 1.04 | 0.15 |

Data Plot and Equation





ITE Land Use Code 931 – Fine Dining Restaurant



Land Use: 931 Fine Dining Restaurant

Description

A fine dining restaurant is a full-service eating establishment with a typical duration of stay of at least 1 hour. A fine dining restaurant generally does not serve breakfast; some do not serve lunch; all serve dinner. This type of restaurant often requests and sometimes requires a reservation and is generally not part of a chain. A patron commonly waits to be seated, is served by wait staff, orders from a menu and pays after the meal. Some of the study sites have lounge or bar facilities (serving alcoholic beverages), but meal service is the primary draw to the restaurant. Fast casual restaurant (Land Use 930) and high-turnover (sit-down) restaurant (Land Use 932) are related uses.

Additional Data

If the fine dining restaurant has outdoor seating, its area is not included in the overall gross floor area. For a restaurant that has significant outdoor seating, the number of seats may be more reliable than GFA as an independent variable on which to establish a trip generation rate.

The sites were surveyed in the 1980s, the 1990s, and the 2010s in Alberta (CAN), California, Colorado, Florida, Indiana, Kentucky, New Jersey, and Utah.

Source Numbers

126, 260, 291, 301, 338, 339, 368, 437, 440, 976, 1053

Fine Dining Restaurant (931)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 19

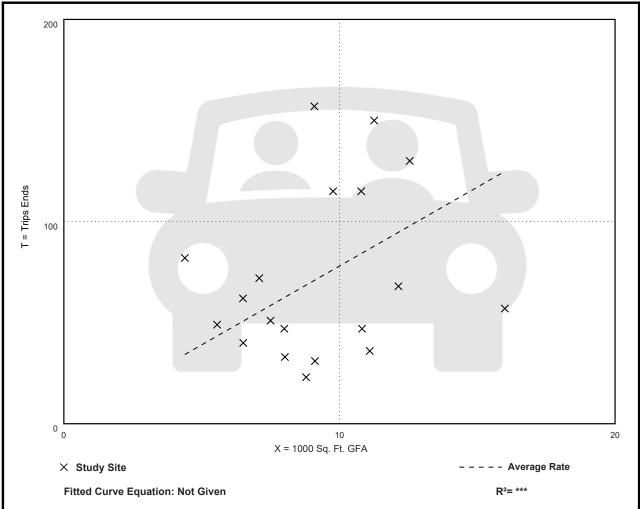
Avg. 1000 Sq. Ft. GFA: 9

Directional Distribution: 67% entering, 33% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 7.80 | 2.62 - 18.68 | 4.49 |

Data Plot and Equation





APPENDIX D – Operational Analysis

Existing Conditions

Cranston Street at Dyer Avenue

Future No Build Conditions

Cranston Street at Dyer Avenue

Future Build Conditions

- Cranston Street at Eastern Driveway
- Cranston Street at Western Driveway
- Dyer Avenue at Southern Driveway



D

Existing Weekday AM / PM Peak Hour

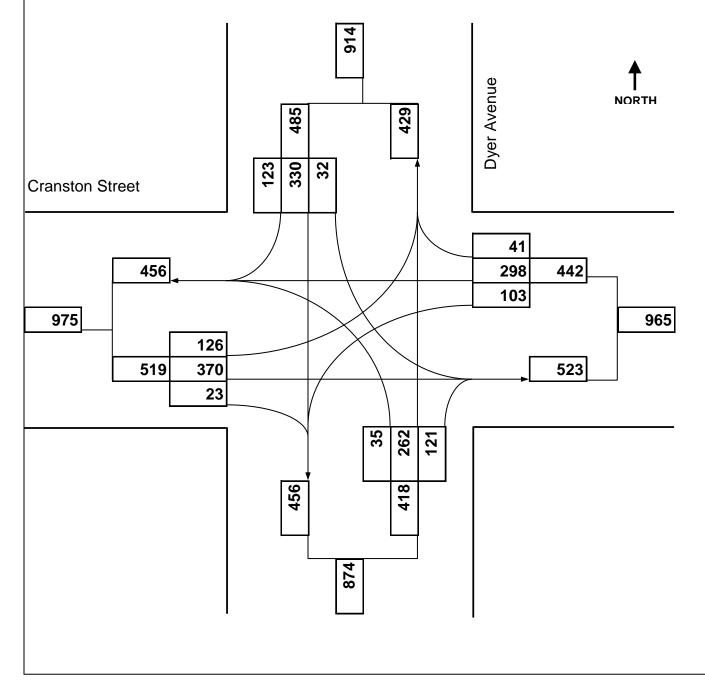






Turning Movement Diagram

| Major Street: | Cranston Street | Minor Street: | Dyer Avenue |
|----------------|-----------------|---------------|-------------------|
| City/Town: | Cranston, RI | Day of Week: | Weekday |
| Reference No.: | 10813 | Peak Period: | 7:30 AM - 8:30 AM |
| Existing: | AM Peak Hour | Future: | n/a |



Cranston Street Mixed Use 3: Dyer Avenue & Cranston Street

| | ۶ | - | \mathbf{r} | ∢ | ← | * | • | Ť | ۲ | 1 | Ļ | ~ |
|-------------------------------|------------|-----------|--------------|------------|------------|------------|------|-------|-----|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | \$ | | | र्स | 1 |
| Traffic Volume (vph) | 126 | 370 | 23 | 103 | 298 | 41 | 35 | 262 | 121 | 32 | 330 | 123 |
| Future Volume (vph) | 126 | 370 | 23 | 103 | 298 | 41 | 35 | 262 | 121 | 32 | 330 | 123 |
| Satd. Flow (prot) | 0 | 1847 | 0 | 0 | 1823 | 0 | 0 | 1770 | 0 | 0 | 1870 | 1568 |
| Flt Permitted | | 0.767 | | | 0.765 | | | 0.900 | | | 0.933 | |
| Satd. Flow (perm) | 0 | 1434 | 0 | 0 | 1410 | 0 | 0 | 1599 | 0 | 0 | 1752 | 1568 |
| Satd. Flow (RTOR) | | 5 | | | 10 | | | 33 | | | | 114 |
| Lane Group Flow (vph) | 0 | 596 | 0 | 0 | 508 | 0 | 0 | 480 | 0 | 0 | 416 | 141 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | 6 |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | 30.0 |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| Act Effct Green (s) | | 29.5 | | | 29.5 | | | 21.5 | | | 21.5 | 21.5 |
| Actuated g/C Ratio | | 0.48 | | | 0.48 | | | 0.35 | | | 0.35 | 0.35 |
| v/c Ratio | | 0.86 | | | 0.74 | | | 0.83 | | | 0.68 | 0.23 |
| Control Delay | | 29.7 | | | 21.2 | | | 32.5 | | | 24.8 | 6.3 |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| Total Delay | | 29.7 | | | 21.2 | | | 32.5 | | | 24.8 | 6.3 |
| LOS | | С | | | С | | | С | | | С | A |
| Approach Delay | | 29.7 | | | 21.2 | | | 32.5 | | | 20.1 | |
| Approach LOS | | С | | | С | | | С | | | С | |
| Queue Length 50th (ft) | | 204 | | | 157 | | | 171 | | | 148 | 7 |
| Queue Length 95th (ft) | | #376 | | | 255 | | | #308 | | | 230 | 38 |
| Internal Link Dist (ft) | | 393 | | | 584 | | | 319 | | | 458 | |
| Turn Bay Length (ft) | | | | | | | | | | | | 80 |
| Base Capacity (vph) | | 857 | | | 845 | | | 700 | | | 746 | 733 |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Reduced v/c Ratio | | 0.70 | | | 0.60 | | | 0.69 | | | 0.56 | 0.19 |
| Intersection Summary | | | | | | | | | | | | |
| Cycle Length: 70 | | | | | | | | | | | | |
| Actuated Cycle Length: 61.5 | | | | | | | | | | | | |
| Control Type: Actuated-Unc | oordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 0.86 | | | | | | | | | | | | |
| Intersection Signal Delay: 25 | | | | | tersection | | _ | | | | | |
| Intersection Capacity Utiliza | tion 92.5% |) | | IC | CU Level | of Service | e F | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |
| # 95th percentile volume e | | | leue may | / be longe | er. | | | | | | | |
| Queue shown is maximu | m after tw | o cycles. | | | | | | | | | | |

Splits and Phases: 3: Dyer Avenue & Cranston Street

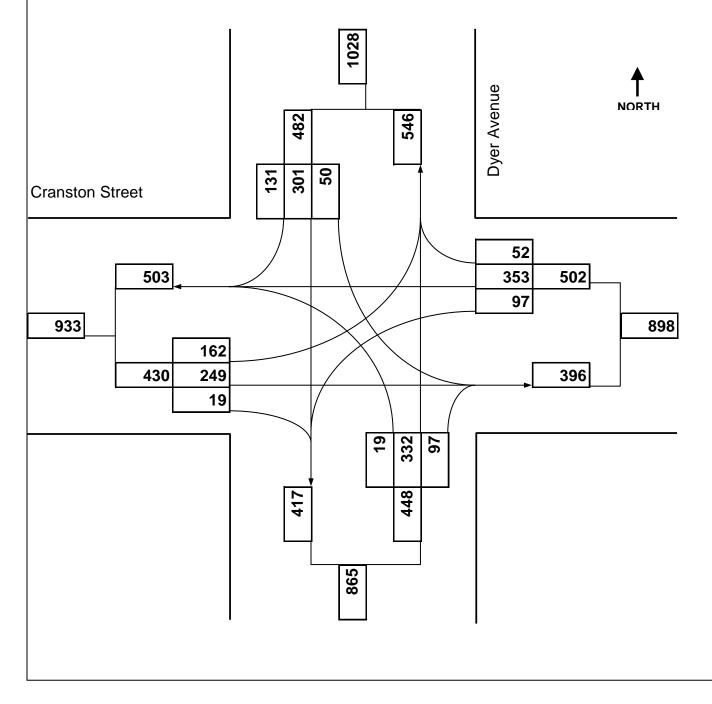
| ₫ ø2 | <u>→</u> _{Ø4} | |
|--------------------------|------------------------|--|
| 30 s | 40 s | |
| ↓ ∞ _{Ø6} | ₩ Ø8 | |
| 30 s | 40 s | |

Timing Plan: AM Peak - Controller Settings



Turning Movement Diagram

| Major Street: | Cranston Street | Minor Street: Dyer Avenue |
|----------------|-----------------|--------------------------------|
| City/Town: | Cranston, RI | Day of Week: Weekday |
| Reference No.: | 10813 | Peak Period: 4:00 PM - 5:00 PM |
| Existing: | PM Peak Hour | Future : n/a |
| | | |



Cranston Street Mixed Use 3: Dyer Avenue & Cranston Street

| WBL 97 97 0 0 0 Perm | WBT 353 353 1834 0.851 1576 12 529 | WBR 52 52 0 | NBL 19 19 0 | NBT 332 332 1819 0.975 | NBR 97 97 0 | SBL 50 50 0 | SBT 4 301 301 | SBR |
|--|---|----------------------|----------------------|------------------------------------|------------------------|------------------------|------------------------|------------------------|
| 97 0 0 Perm | 353 353 1834 0.851 1576 12 529 | 52 0 | 19 0 | 332 332 1819 0.975 | 97 | 50 | 301 | |
| 97 0 0 Perm | 353 353 1834 0.851 1576 12 529 | 52 0 | 19 0 | 332 1819 0.975 | 97 | 50 | | |
| 0 0 Perm | 1834 0.851 1576 12 529 | 0 | 0 | 1819 0.975 | | | 301 | 131 |
| 0 0 Perm | 0.851 1576 12 529 | | | 0.975 | 0 | 0 | | 13 |
| 0 Perm | 1576 12 529 | 0 | 0 | | | 5 | 1860 | 1615 |
| 0 Perm | 12 529 | 0 | 0 | | | | 0.875 | |
| Perm | 529 | | | 1777 | 0 | 0 | 1639 | 1579 |
| Perm | | | | 22 | | | | 125 |
| | | 0 | 0 | 471 | 0 | 0 | 370 | 138 |
| 8 | NA | | Perm | NA | | Perm | NA | Perm |
| 8 | 8 | | | 2 | | | 6 | |
| | | | 2 | | | 6 | | 6 |
| 40.0 | 40.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | 30.0 |
| | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| | 25.8 | | | 19.1 | | | 19.1 | 19.1 |
| | 0.46 | | | 0.34 | | | 0.34 | 0.34 |
| | 0.72 | | | 0.76 | | | 0.66 | 0.22 |
| | 18.6 | | | 25.9 | | | 23.5 | 5.3 |
| | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| | 18.6 | | | 25.9 | | | 23.5 | 5.3 |
| | В | | | С | | | С | A |
| | 18.6 | | | 25.9 | | | 18.5 | |
| | В | | | С | | | В | |
| | 135 | | | 135 | | | 107 | 3 |
| | 262 | | | #274 | | | 216 | 37 |
| | 584 | | | 319 | | | 458 | |
| | | | | | | | | 80 |
| | 1063 | | | 872 | | | 794 | 829 |
| | 0 | | | 0 | | | 0 | (|
| | 0 | | | 0 | | | 0 | (|
| | 0 | | | 0 | | | 0 | C |
| | 0.50 | | | 0.54 | | | 0.47 | 0.17 |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| 16 | CU Level | of Service | Ε | | | | | |
| N | | | | | | | | |
| | er. | | | | | | | |
| | 10 | | | ICU Level of Service E | ICU Level of Service E | ICU Level of Service E | ICU Level of Service E | ICU Level of Service E |

Splits and Phases: 3: Dyer Avenue & Cranston Street

| d Ø2 | | |
|-------|---------|--|
| 30 s | 40 s | |
| \$ Ø6 | ₩ Ø8 | |
| 30 s | 40 s | |

Timing Plan: PM Peak - Controller Settings

D

Future 2028 No-Build Weekday AM / PM Peak Hour

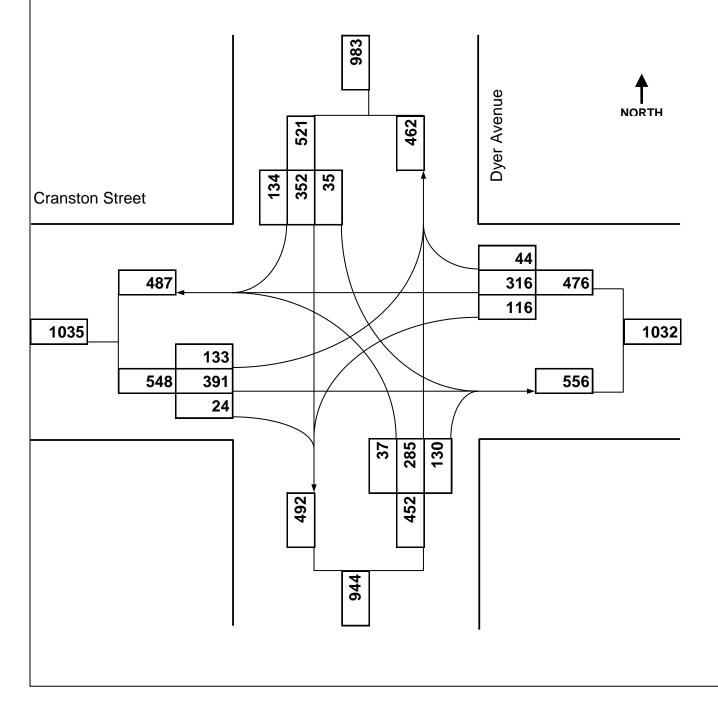






Turning Movement Diagram

| City/Town:Cranston, RIDay of Week: WeekdayReference No.:10813Peak Period:7:30 AM - 8:30 AMExisting:N/AFuture:2028 No Build | Major Street: | Cranston Street | Minor Street: Dyer Avenue |
|--|----------------|-----------------|--------------------------------|
| | City/Town: | Cranston, RI | Day of Week: Weekday |
| Existing: N/A Euture: 2028 No Build | Reference No.: | 10813 | Peak Period: 7:30 AM - 8:30 AM |
| | Existing: | N/A | Future: 2028 No Build |



Cranston Street Mixed Use 3: Dyer Avenue & Cranston Street

| 5. Dyel Avenue & C | Jiansio | | 51 | | | | | | | - NC | Dullu Al | |
|-------------------------------|-------------|------------|--------------|------------|-------------|------------|------|-------|-----|------|----------|------|
| | ≯ | - | \mathbf{r} | 4 | ← | * | • | 1 | 1 | 1 | Ŧ | ~ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | \$ | | | 4 | | | र्स | 1 |
| Traffic Volume (vph) | 133 | 391 | 24 | 116 | 316 | 44 | 37 | 285 | 130 | 35 | 352 | 134 |
| Future Volume (vph) | 133 | 391 | 24 | 116 | 316 | 44 | 37 | 285 | 130 | 35 | 352 | 134 |
| Satd. Flow (prot) | 0 | 1847 | 0 | 0 | 1819 | 0 | 0 | 1770 | 0 | 0 | 1870 | 1568 |
| Flt Permitted | | 0.742 | | | 0.727 | | | 0.845 | | | 0.921 | |
| Satd. Flow (perm) | 0 | 1387 | 0 | 0 | 1338 | 0 | 0 | 1502 | 0 | 0 | 1729 | 1568 |
| Satd. Flow (RTOR) | | 5 | | | 11 | | | 32 | | | | 116 |
| Lane Group Flow (vph) | 0 | 630 | 0 | 0 | 547 | 0 | 0 | 520 | 0 | 0 | 445 | 154 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | 6 |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | 30.0 |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| Act Effct Green (s) | | 32.8 | | | 32.8 | | | 24.6 | | | 24.6 | 24.6 |
| Actuated g/C Ratio | | 0.49 | | | 0.49 | | | 0.36 | | | 0.36 | 0.36 |
| v/c Ratio | | 0.93 | | | 0.83 | | | 0.92 | | | 0.71 | 0.24 |
| Control Delay | | 39.8 | | | 28.3 | | | 44.7 | | | 26.6 | 6.6 |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| Total Delay | | 39.8 | | | 28.3 | | | 44.7 | | | 26.6 | 6.6 |
| LOS | | D | | | С | | | D | | | С | A |
| Approach Delay | | 39.8 | | | 28.3 | | | 44.7 | | | 21.5 | |
| Approach LOS | | D | | | С | | | D | | | С | |
| Queue Length 50th (ft) | | 230 | | | 182 | | | 200 | | | 162 | 11 |
| Queue Length 95th (ft) | | #422 | | | #346 | | | #367 | | | 252 | 43 |
| Internal Link Dist (ft) | | 393 | | | 584 | | | 319 | | | 458 | |
| Turn Bay Length (ft) | | | | | | | | | | | | 80 |
| Base Capacity (vph) | | 727 | | | 704 | | | 580 | | | 645 | 657 |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Reduced v/c Ratio | | 0.87 | | | 0.78 | | | 0.90 | | | 0.69 | 0.23 |
| Intersection Summary | | | | | | | | | | | | |
| Cycle Length: 70 | | | | | | | | | | | | |
| Actuated Cycle Length: 67.4 | 4 | | | | | | | | | | | |
| Control Type: Actuated-Unc | coordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 0.93 | | | | | | | | | | | | |
| Intersection Signal Delay: 33 | 3.4 | | | Ir | ntersection | n LOS: C | | | | | | |
| Intersection Capacity Utiliza | |) | | IC | CU Level | of Service | e F | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |
| # 95th percentile volume e | exceeds ca | apacity, q | ueue may | / be longe | er. | | | | | | | |
| Queue shown is maximu | | | | | | | | | | | | |
| | | 2 | | | | | | | | | | |

Splits and Phases: 3: Dyer Avenue & Cranston Street

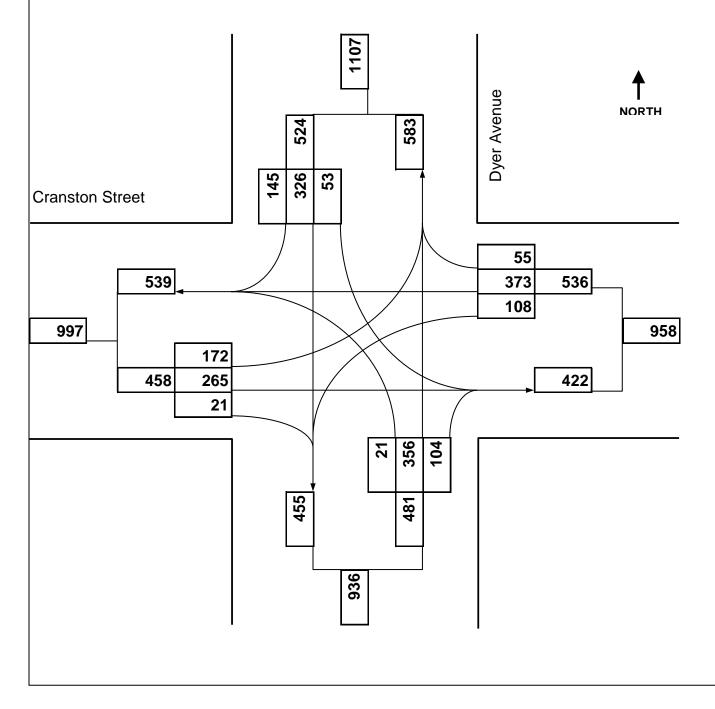
| ₫ ø2 | <u>→</u> _{Ø4} | |
|--------------------------|------------------------|--|
| 30 s | 40 s | |
| ↓ ∞ _{Ø6} | ₩ Ø8 | |
| 30 s | 40 s | |

Timing Plan: AM Peak - Controller Settings



Turning Movement Diagram

| Major Street: | Cranston Street | Minor Street: Dyer Avenue |
|----------------|-----------------|--------------------------------|
| City/Town: | Cranston, RI | Day of Week: Weekday |
| Reference No.: | 10813 | Peak Period: 4:00 PM - 5:00 PM |
| Existing: | N/A | Future: 2028 No Build |
| | | |



Cranston Street Mixed Use 3: Dyer Avenue & Cranston Street

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|--------------------------------|-----------|-------------|--------------|----------|-------------|------------|------|-------|-----|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | | | र्स | 1 |
| Traffic Volume (vph) | 172 | 265 | 21 | 109 | 373 | 55 | 21 | 356 | 104 | 53 | 326 | 145 |
| Future Volume (vph) | 172 | 265 | 21 | 109 | 373 | 55 | 21 | 356 | 104 | 53 | 326 | 145 |
| Satd. Flow (prot) | 0 | 1825 | 0 | 0 | 1834 | 0 | 0 | 1819 | 0 | 0 | 1860 | 1615 |
| Flt Permitted | | 0.627 | | | 0.830 | | | 0.973 | | | 0.850 | |
| Satd. Flow (perm) | 0 | 1165 | 0 | 0 | 1537 | 0 | 0 | 1774 | 0 | 0 | 1592 | 1579 |
| Satd. Flow (RTOR) | | 5 | | | 12 | | | 22 | | | | 129 |
| Lane Group Flow (vph) | 0 | 482 | 0 | 0 | 566 | 0 | 0 | 506 | 0 | 0 | 399 | 153 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | 6 |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | 30.0 |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| Act Effct Green (s) | | 29.0 | | | 29.0 | | | 20.9 | | | 20.9 | 20.9 |
| Actuated g/C Ratio | | 0.48 | | | 0.48 | | | 0.35 | | | 0.35 | 0.35 |
| v/c Ratio | | 0.86 | | | 0.76 | | | 0.81 | | | 0.73 | 0.24 |
| Control Delay | | 32.1 | | | 21.1 | | | 30.2 | | | 27.5 | 5.9 |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| Total Delay | | 32.1 | | | 21.1 | | | 30.2 | | | 27.5 | 5.9 |
| LOS | | С | | | С | | | С | | | С | А |
| Approach Delay | | 32.1 | | | 21.1 | | | 30.2 | | | 21.5 | |
| Approach LOS | | С | | | С | | | С | | | С | |
| Queue Length 50th (ft) | | 164 | | | 176 | | | 182 | | | 144 | 7 |
| Queue Length 95th (ft) | | #345 | | | 299 | | | #334 | | | #244 | 42 |
| Internal Link Dist (ft) | | 393 | | | 584 | | | 319 | | | 458 | |
| Turn Bay Length (ft) | | | | | | | | | | | | 80 |
| Base Capacity (vph) | | 713 | | | 943 | | | 785 | | | 694 | 761 |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Reduced v/c Ratio | | 0.68 | | | 0.60 | | | 0.64 | | | 0.57 | 0.20 |
| Intersection Summary | | | | | | | | | | | | |
| Cycle Length: 70 | | | | | | | | | | | | |
| Actuated Cycle Length: 60.5 | | | | | | | | | | | | |
| Control Type: Actuated-Unco | ordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 0.86 | | | | | | | | | | | | |
| Intersection Signal Delay: 25 | .9 | | | In | itersection | 1 LOS: C | | | | | | |
| Intersection Capacity Utilizat | |) | | IC | CU Level | of Service | e F | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |
| # 95th percentile volume e | xceeds ca | apacity, qu | leue may | be longe | er. | | | | | | | |
| Queue shown is maximur | | | | | | | | | | | | |

Splits and Phases: 3: Dyer Avenue & Cranston Street

| ↑ ø2 | | |
|---------------|---------|--|
| 30 s | 40 s | |
| \$ ∞ø6 | ₩ Ø8 | |
| 30 s | 40 s | |

Timing Plan: PM Peak - Controller Settings

D

Future 2028 Build Weekday AM / PM Peak Hour

- Cranston Street at Dyer Avenue
- Cranston Street at Eastern Driveway
- Cranston Street at Western Driveway
 - Dyer Avenue at Southern Driveway

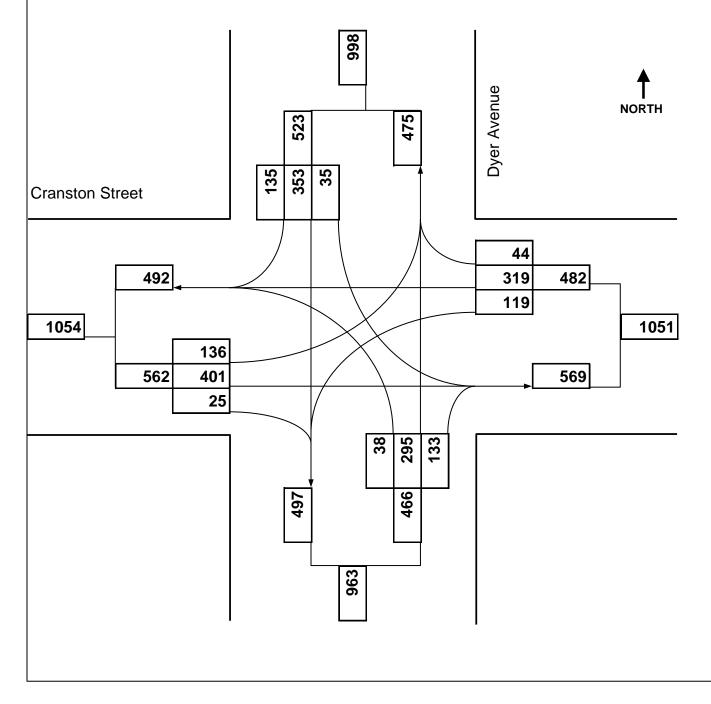






Turning Movement Diagram

| Major Street: | Cranston Street | Minor Street: Dyer Avenue |
|----------------|-----------------|--------------------------------|
| City/Town: | Cranston, RI | Day of Week: Weekday |
| Reference No.: | 10813 | Peak Period: 7:30 AM - 8:30 AM |
| Existing: | N/A | Future: 2028 Build |



Cranston Street Mixed Use 3: Dyer Avenue & Cranston Street

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|--------------------------------|------------|-------------|--------------|----------|-------------|------------|------|-------|-----|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | \$ | | | र्स | 7 |
| Traffic Volume (vph) | 136 | 401 | 25 | 119 | 319 | 44 | 38 | 295 | 133 | 35 | 353 | 135 |
| Future Volume (vph) | 136 | 401 | 25 | 119 | 319 | 44 | 38 | 295 | 133 | 35 | 353 | 135 |
| Satd. Flow (prot) | 0 | 1847 | 0 | 0 | 1821 | 0 | 0 | 1770 | 0 | 0 | 1870 | 1568 |
| Flt Permitted | | 0.739 | | | 0.715 | | | 0.835 | | | 0.916 | |
| Satd. Flow (perm) | 0 | 1381 | 0 | 0 | 1317 | 0 | 0 | 1484 | 0 | 0 | 1720 | 1568 |
| Satd. Flow (RTOR) | | 5 | | | 10 | | | 32 | | | | 117 |
| Lane Group Flow (vph) | 0 | 646 | 0 | 0 | 555 | 0 | 0 | 536 | 0 | 0 | 446 | 155 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | 6 |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | 30.0 |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| Act Effct Green (s) | | 33.5 | | | 33.5 | | | 25.0 | | | 25.0 | 25.0 |
| Actuated g/C Ratio | | 0.49 | | | 0.49 | | | 0.36 | | | 0.36 | 0.36 |
| v/c Ratio | | 0.95 | | | 0.86 | | | 0.95 | | | 0.71 | 0.24 |
| Control Delay | | 44.4 | | | 30.7 | | | 51.8 | | | 26.9 | 6.5 |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| Total Delay | | 44.4 | | | 30.7 | | | 51.8 | | | 26.9 | 6.5 |
| LOS | | D | | | С | | | D | | | С | А |
| Approach Delay | | 44.4 | | | 30.7 | | | 51.8 | | | 21.6 | |
| Approach LOS | | D | | | С | | | D | | | С | |
| Queue Length 50th (ft) | | 243 | | | 189 | | | 212 | | | 163 | 11 |
| Queue Length 95th (ft) | | #439 | | | #360 | | | #388 | | | 253 | 44 |
| Internal Link Dist (ft) | | 128 | | | 584 | | | 490 | | | 458 | |
| Turn Bay Length (ft) | | | | | | | | | | | | 80 |
| Base Capacity (vph) | | 709 | | | 678 | | | 562 | | | 628 | 647 |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Reduced v/c Ratio | | 0.91 | | | 0.82 | | | 0.95 | | | 0.71 | 0.24 |
| Intersection Summary | | | | | | | | | | | | |
| Cycle Length: 70 | | | | | | | | | | | | |
| Actuated Cycle Length: 68.5 | | | | | | | | | | | | |
| Control Type: Actuated-Unco | ordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 0.95 | | | | | | | | | | | | |
| Intersection Signal Delay: 37 | .0 | | | In | itersectior | ו LOS: D | | | | | | |
| Intersection Capacity Utilizat | ion 98.7% |) | | IC | CU Level | of Service | e F | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |
| # 95th percentile volume e | xceeds ca | ipacity, qu | ueue may | be longe | er. | | | | | | | |
| Queue shown is maximur | n after tw | o cycles. | | | | | | | | | | |

Splits and Phases: 3: Dyer Avenue & Cranston Street

| √ <i>ø</i> 2 | A ₀₄ | |
|-------------------------|-----------------|--|
| 30 s | 40 s | |
| ↓ ø ₆ | ↓ Ø8 | |
| 30 s | 40 s | |

Timing Plan: AM Peak - Controller Settings

Cranston Street Mixed-Use

| Cranston, RI |
|--------------|
|--------------|

| | ٦ | - | \mathbf{F} | ∢ | ← | • | • | Ť | ۲ | 5 | Ŧ | ~ |
|---|---|---|--------------|--|---|------------|------|--|-----|------|--|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ľ | el | | ۲ | et | | | ÷ | | | र्स | 1 |
| Traffic Volume (vph) | 136 | 401 | 25 | 119 | 319 | 44 | 38 | 295 | 133 | 35 | 353 | 135 |
| Future Volume (vph) | 136 | 401 | 25 | 119 | 319 | 44 | 38 | 295 | 133 | 35 | 353 | 135 |
| Satd. Flow (prot) | 1805 | 1858 | 0 | 1736 | 1844 | 0 | 0 | 1770 | 0 | 0 | 1870 | 1568 |
| Flt Permitted | 0.380 | | | 0.297 | | | | 0.939 | | | 0.926 | |
| Satd. Flow (perm) | 721 | 1858 | 0 | 542 | 1844 | 0 | 0 | 1669 | 0 | 0 | 1739 | 1568 |
| Satd. Flow (RTOR) | | 7 | | | 15 | | | 26 | | | | 94 |
| Lane Group Flow (vph) | 156 | 490 | 0 | 137 | 418 | 0 | 0 | 536 | 0 | 0 | 446 | 155 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | 6 |
| Total Split (s) | 51.0 | 51.0 | | 51.0 | 51.0 | | 29.0 | 29.0 | | 29.0 | 29.0 | 29.0 |
| Total Lost Time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| Act Effct Green (s) | 20.2 | 20.2 | | 20.2 | 20.2 | | | 24.3 | | | 24.3 | 24.3 |
| Actuated g/C Ratio | 0.37 | 0.37 | | 0.37 | 0.37 | | | 0.45 | | | 0.45 | 0.45 |
| v/c Ratio | 0.59 | 0.71 | | 0.69 | 0.61 | | | 0.71 | | | 0.58 | 0.21 |
| Control Delay | 23.2 | 20.3 | | 32.9 | 17.0 | | | 20.9 | | | 16.8 | 6.4 |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| Total Delay | 23.2 | 20.3 | | 32.9 | 17.0 | | | 20.9 | | | 16.8 | 6.4 |
| LOS | С | С | | С | В | | | С | | | В | A |
| Approach Delay | | 21.0 | | | 20.9 | | | 20.9 | | | 14.1 | |
| Approach LOS | | С | | | С | | | С | | | В | |
| Queue Length 50th (ft) | 39 | 128 | | 36 | 101 | | | 125 | | | 101 | 11 |
| Queue Length 95th (ft) | 84 | 198 | | 87 | 161 | | | #325 | | | 226 | 47 |
| Internal Link Dist (ft) | | 197 | | | 584 | | | 491 | | | 458 | |
| Turn Bay Length (ft) | 125 | | | 150 | | | | | | | | 80 |
| Base Capacity (vph) | 615 | 1586 | | 462 | 1575 | | | 757 | | | 774 | 750 |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | | 0 | | | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | | 0 | | | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | | 0 | | | 0 | 0 |
| Reduced v/c Ratio | 0.25 | 0.31 | | 0.30 | 0.27 | | | 0.71 | | | 0.58 | 0.21 |
| Intersection Summary | | | | | | | | | | | | |
| Cycle Length: 80 | | | | | | | | | | | | |
| Actuated Cycle Length: 54.6 | ,) | | | | | | | | | | | |
| Control Type: Actuated-Unc | oordinated | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Intersection Signal Delay: 19 | | | | | tersectior | | | | | | | |
| Intersection Capacity Utiliza | tion 92.2% | | | IC | U Level | of Service | e F | | | | | |
| | | | | | | | | | | | | |
| Total Split (s) Total Lost Time (s) Act Effct Green (s) Actuated g/C Ratio v/c Ratio Control Delay Queue Delay Total Delay LOS Approach Delay Approach Delay Approach LOS Queue Length 50th (ft) Queue Length 95th (ft) Internal Link Dist (ft) Turn Bay Length (ft) Base Capacity (vph) Starvation Cap Reductn Spillback Cap Reductn Storage Cap Reductn Storage Cap Reductn Reduced v/c Ratio Intersection Summary Cycle Length: 80 Actuated Cycle Length: 54.6 Control Type: Actuated-Unc Maximum v/c Ratio: 0.71 Intersection Signal Delay: 19 | 51.0 5.0 20.2 0.37 0.59 23.2 0.0 23.2 C 39 84 125 615 0 0 0 0.25 5 5 00rdinated 9.2 tion 92.2% | 5.0 20.2 0.37 0.71 20.3 0.0 20.3 C 21.0 C 128 198 197 1586 0 0 0 0 0.31 | | 51.0 5.0 20.2 0.37 0.69 32.9 0.0 32.9 C 36 87 150 462 0 0 0 0.30 | 5.0 20.2 0.37 0.61 17.0 0.0 17.0 B 20.9 C 101 161 584 1575 0 0 0 0 0.27 | | 29.0 | 5.0 24.3 0.45 0.71 20.9 0.0 20.9 C 20.9 C 20.9 C 125 #325 491 757 0 0 0 0 | | | 5.0 24.3 0.45 0.58 16.8 0.0 16.8 B 14.1 B 101 226 458 774 0 0 0 0 | 29.0 5.0 24.3 0.45 0.21 6.4 0.0 6.4 A A 11 47 80 750 0 0 0 0 0 |

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 3: Dyer Avenue & Cranston Street

| ↑ _{Ø2} | |
|------------------------|---------|
| 29 s | 51s |
| | ₩ Ø8 |
| 29 s | 51s |

Future Build with Left Lanes Timing Plan: AM Peak



Turning Movement Diagram

| Major Street: | Cranston Street | Minor Street: | |
|-----------------|----------------------|-----------------------|------------------------------------|
| City/Town: | Cranston, RI | Day of Week: | - |
| Reference No.: | 10813 | Peak Period: | 4:00 PM - 5:00 PM |
| Existing: | n/a | Future: | 2028 Build |
| Cranston Street | 151 337 541 53 | 592 | Dyer Avenue |
| 1036 471 | 176 | | 55 391 558 112 989 431 |
| | 472 | 962 490 361 106 | |

Cranston Street Mixed Use 3: Dyer Avenue & Cranston Street

| | ≯ | - | \rightarrow | - | - | • | 1 | † | 1 | × | + | - |
|---|----------|---------------------|---------------|------------------------|-------|-----|------|----------|-----|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBF |
| Lane Configurations | | \$ | | | \$ | | | 4 | | | र्च | 1 |
| Traffic Volume (vph) | 176 | 272 | 23 | 112 | 391 | 55 | 23 | 361 | 106 | 53 | 337 | 151 |
| Future Volume (vph) | 176 | 272 | 23 | 112 | 391 | 55 | 23 | 361 | 106 | 53 | 337 | 151 |
| Satd. Flow (prot) | 0 | 1823 | 0 | 0 | 1836 | 0 | 0 | 1819 | 0 | 0 | 1860 | 1615 |
| Flt Permitted | | 0.616 | | | 0.826 | | | 0.970 | | | 0.844 | |
| Satd. Flow (perm) | 0 | 1143 | 0 | 0 | 1532 | 0 | 0 | 1768 | 0 | 0 | 1581 | 1579 |
| Satd. Flow (RTOR) | | 5 | | | 11 | | | 22 | | | | 130 |
| Lane Group Flow (vph) | 0 | 495 | 0 | 0 | 588 | 0 | 0 | 516 | 0 | 0 | 411 | 159 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | 6 |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | 30.0 |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| Act Effct Green (s) | | 30.3 | | | 30.3 | | | 21.4 | | | 21.4 | 21.4 |
| Actuated g/C Ratio | | 0.49 | | | 0.49 | | | 0.34 | | | 0.34 | 0.34 |
| v/c Ratio | | 0.88 | | | 0.78 | | | 0.83 | | | 0.76 | 0.25 |
| Control Delay | | 35.4 | | | 22.4 | | | 32.2 | | | 29.5 | 6.1 |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| Total Delay | | 35.4 | | | 22.4 | | | 32.2 | | | 29.5 | 6.1 |
| LOS | | D | | | С | | | С | | | С | A |
| Approach Delay | | 35.4 | | | 22.4 | | | 32.2 | | | 23.0 | |
| Approach LOS | | D | | | С | | | С | | | С | |
| Queue Length 50th (ft) | | 174 | | | 188 | | | 188 | | | 151 | 8 |
| Queue Length 95th (ft) | | #363 | | | #337 | | | #346 | | | #278 | 44 |
| Internal Link Dist (ft) | | 128 | | | 584 | | | 490 | | | 458 | |
| Turn Bay Length (ft) | | | | | | | | | | | | 80 |
| Base Capacity (vph) | | 672 | | | 902 | | | 752 | | | 661 | 736 |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | C |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | C |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | 0 |
| Reduced v/c Ratio | | 0.74 | | | 0.65 | | | 0.69 | | | 0.62 | 0.22 |
| Intersection Summary | | | | | | | | | | | | |
| Cycle Length: 70 | | | | | | | | | | | | |
| Actuated Cycle Length: 62.1 | | | | | | | | | | | | |
| Control Type: Actuated-Uncoo | rdinated | | | | | | | | | | | |
| Maximum v/c Ratio: 0.88 | | | | | | | | | | | | |
| Intersection Signal Delay: 27.9 | | Intersection LOS: C | | | | | | | | | | |
| Intersection Capacity Utilization 98.3% | | | | ICU Level of Service F | | | | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |
| # 95th percentile volume exc | ceeds ca | apacity, qu | Leue may | v be longe | er. | | | | | | | |

Splits and Phases: 3: Dyer Avenue & Cranston Street

| ₫ _{Ø2} | -A-04 | |
|------------------------|---------|--|
| 30 s | 40 s | |
| \$ Ø6 | ₩ Ø8 | |
| 30 s | 40 s | |

Timing Plan: PM Peak - Controller Settings

Cranston Street Mixed-Use

| Cranston, R |
|-------------|
|-------------|

| | ≯ | - | \mathbf{F} | 4 | + | • | • | Ť | 1 | 1 | ŧ | ~ |
|-------------------------------|--------------|-----------|--------------|----------|------------|------------|------|-------|-----|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | eî 👘 | | ሻ | 4 | | | 4 | | | र्भ | 1 |
| Traffic Volume (vph) | 176 | 272 | 23 | 112 | 391 | 55 | 23 | 361 | 106 | 53 | 337 | 151 |
| Future Volume (vph) | 176 | 272 | 23 | 112 | 391 | 55 | 23 | 361 | 106 | 53 | 337 | 151 |
| Satd. Flow (prot) | 1787 | 1840 | 0 | 1787 | 1843 | 0 | 0 | 1819 | 0 | 0 | 1860 | 1615 |
| Flt Permitted | 0.359 | | | 0.536 | | | | 0.971 | | | 0.891 | |
| Satd. Flow (perm) | 675 | 1840 | 0 | 1005 | 1843 | 0 | 0 | 1770 | 0 | 0 | 1669 | 1578 |
| Satd. Flow (RTOR) | | 8 | | | 13 | | | 20 | | | | 115 |
| Lane Group Flow (vph) | 185 | 310 | 0 | 118 | 470 | 0 | 0 | 516 | 0 | 0 | 411 | 159 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | 6 |
| Total Split (s) | 46.0 | 46.0 | | 46.0 | 46.0 | | 34.0 | 34.0 | | 34.0 | 34.0 | 34.0 |
| Total Lost Time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | | 5.0 | | | 5.0 | 5.0 |
| Act Effct Green (s) | 21.1 | 21.1 | | 21.1 | 21.1 | | | 20.4 | | | 20.4 | 20.4 |
| Actuated g/C Ratio | 0.40 | 0.40 | | 0.40 | 0.40 | | | 0.39 | | | 0.39 | 0.39 |
| v/c Ratio | 0.68 | 0.42 | | 0.29 | 0.63 | | | 0.74 | | | 0.63 | 0.23 |
| Control Delay | 28.3 | 13.2 | | 13.6 | 16.8 | | | 22.1 | | | 19.6 | 6.1 |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 | | | 0.0 | 0.0 |
| Total Delay | 28.3 | 13.2 | | 13.6 | 16.8 | | | 22.1 | | | 19.6 | 6.1 |
| LOS | С | В | | В | В | | | С | | | В | A |
| Approach Delay | | 18.9 | | | 16.1 | | | 22.1 | | | 15.8 | |
| Approach LOS | | В | | | В | | | С | | | В | |
| Queue Length 50th (ft) | 43 | 61 | | 23 | 104 | | | 117 | | | 92 | 8 |
| Queue Length 95th (ft) | 128 | 137 | | 64 | 222 | | | #317 | | | 248 | 49 |
| Internal Link Dist (ft) | | 197 | | | 584 | | | 491 | | | 458 | |
| Turn Bay Length (ft) | 125 | | | 150 | | | | | | | | 80 |
| Base Capacity (vph) | 539 | 1473 | | 803 | 1476 | | | 1078 | | | 1009 | 1000 |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | | 0 | | | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | | 0 | | | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | | 0 | | | 0 | 0 |
| Reduced v/c Ratio | 0.34 | 0.21 | | 0.15 | 0.32 | | | 0.48 | | | 0.41 | 0.16 |
| Intersection Summary | | | | | | | | | | | | |
| Cycle Length: 80 | | | | | | | | | | | | |
| Actuated Cycle Length: 52.4 | | | | | | | | | | | | |
| Control Type: Actuated-Unc | coordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 0.74 | | | | | | | | | | | | |
| Intersection Signal Delay: 1 | | | | | tersectior | | | | | | | |
| Intersection Capacity Utiliza | ation 90.9% | | | IC | CU Level | of Service | Ε | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |
| # 95th percentile volume | | | leue may | be longe | er. | | | | | | | |
| Queue shown is maximu | um after two | o cycles. | | | | | | | | | | |

Splits and Phases: 3: Dyer Avenue & Cranston Street

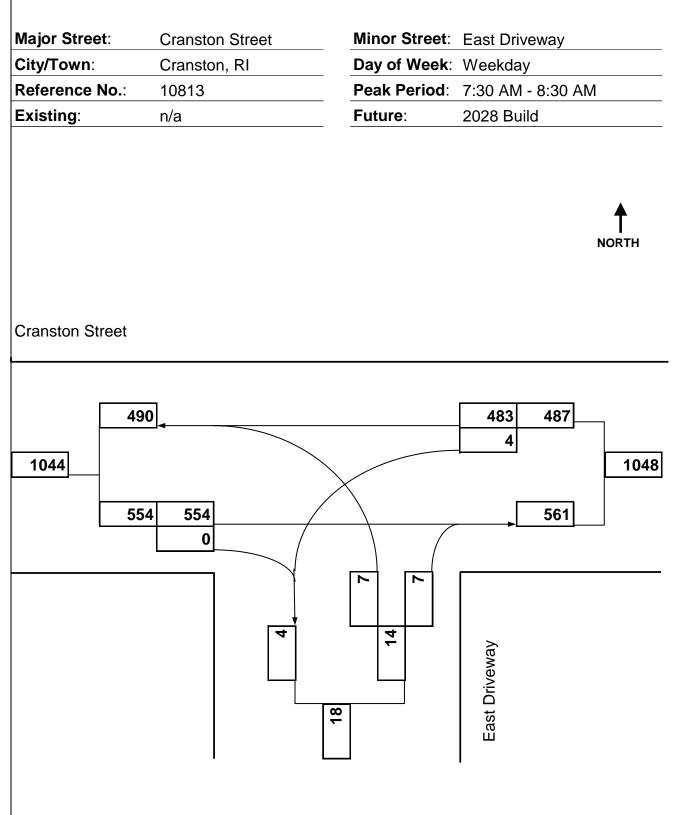
| ▲ ¶ _{Ø2} | <u></u> 4 |
|--------------------------|-------------|
| 34 s | 46 s |
| ↓ Ø6 | ↓ Ø8 |
| 34 s | 46 s |

Future Build - with Left Lanes Timing Plan: PM Peak Cranston, Rhode Island

Cranston Street at Eastern Driveway







| Int Delay, s/veh | 0.3 | | | | | |
|------------------------|------|------|------|------|------|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 4 | | | ्स | ۰¥ | |
| Traffic Vol, veh/h | 554 | 0 | 4 | 483 | 7 | 7 |
| Future Vol, veh/h | 554 | 0 | 4 | 483 | 7 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 602 | 0 | 4 | 525 | 8 | 8 |

| Major/Minor N | Najor1 | Ν | Najor2 | | Vinor1 | |
|-----------------------|--------|-------|--------|-----|-----------|-------|
| Conflicting Flow All | 0 | 0 | 602 | | 1135 | 602 |
| Stage 1 | - | - | - | - | 602 | - |
| Stage 2 | - | - | - | - | 533 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 975 | - | 004 | 500 |
| Stage 1 | - | - | - | - | 547 | - |
| Stage 2 | - | - | - | - | 588 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 975 | - | 223 | 500 |
| Mov Cap-2 Maneuver | - | - | - | - | 223 | - |
| Stage 1 | - | - | - | - | 547 | - |
| Stage 2 | - | - | - | - | 584 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.1 | | 17.3 | |
| HCM LOS | 0 | | 0.1 | | 17.3 C | |
| | | | | | C | |
| | | | | | | |
| Minor Lane/Major Mvm | it N | VBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 308 | - | - | 975 | - |
| HCM Lane V/C Ratio | | 0.049 | - | - | 0.004 | - |
| HCM Control Delay (s) | | 17.3 | - | - | 8.7 | 0 |
| HCM Lane LOS | | С | - | - | А | А |

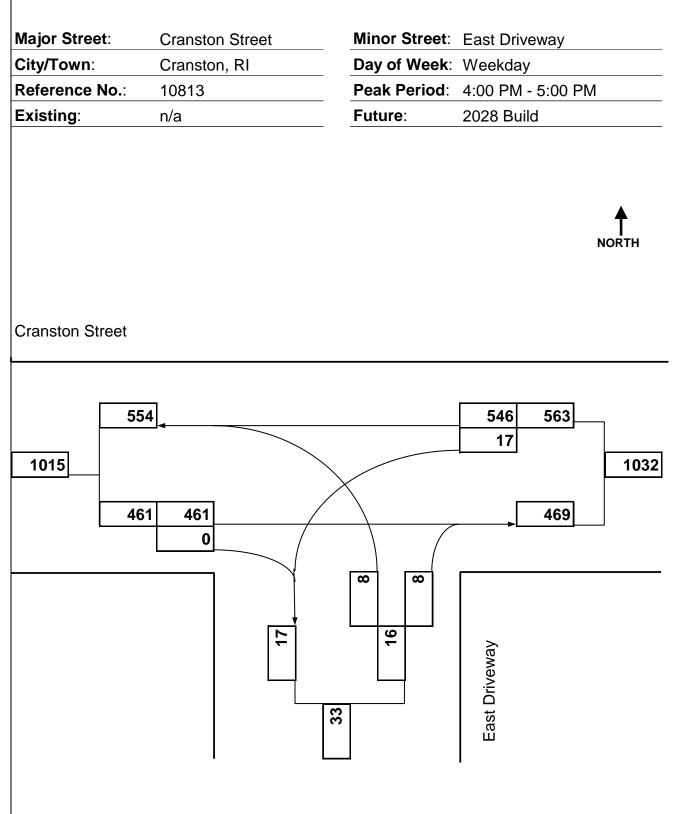
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-

HCM 95th %tile Q(veh)

0.2





| Int Delay, s/veh | 0.4 | | | | | |
|------------------------|------|------|------|--------------|------|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ef 👘 | | | ् | Y | |
| Traffic Vol, veh/h | 461 | 0 | 17 | 546 | 8 | 8 |
| Future Vol, veh/h | 461 | 0 | 17 | 546 | 8 | 8 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 501 | 0 | 18 | 593 | 9 | 9 |

| Major/Minor I | Major1 | Λ | Najor2 | Ν | Minor1 | |
|-----------------------|--------|-------|--------|-----|--------|-------|
| Conflicting Flow All | 0 | 0 | 501 | | 1130 | 501 |
| Stage 1 | - | - | - | - | 501 | - |
| Stage 2 | - | - | - | - | 629 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1063 | - | 225 | 570 |
| Stage 1 | - | - | - | - | 609 | - |
| Stage 2 | - | - | - | - | 531 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1063 | - | 219 | 570 |
| Mov Cap-2 Maneuver | - | - | - | - | 219 | - |
| Stage 1 | - | - | - | - | 609 | - |
| Stage 2 | - | - | - | - | 518 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.3 | | 17.1 | |
| HCM LOS | Ū | | 0.0 | | C | |
| | | | | | Ű | |
| | | | EDT | 500 | | MOT |
| Minor Lane/Major Mvm | nt í | VBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 316 | - | | 1063 | - |
| HCM Lane V/C Ratio | | 0.055 | - | - | 0.017 | - |
| HCM Control Delay (s) |) | 17.1 | - | - | 8.4 | 0 |

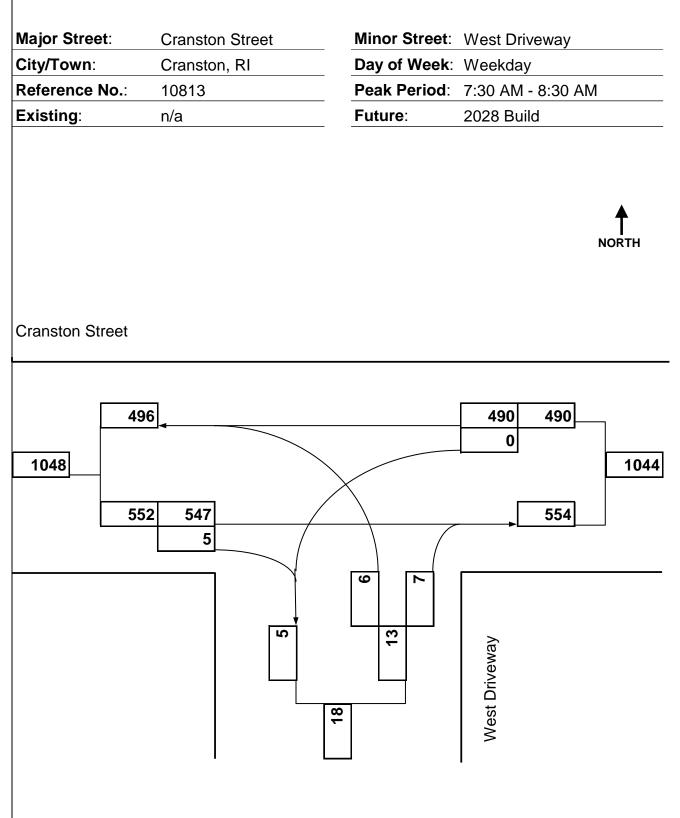
| HCM Control Delay (s) | 17.1 | - | - | 8.4 | 0 |
|-----------------------|------|---|---|-----|---|
| HCM Lane LOS | С | - | - | Α | А |
| HCM 95th %tile Q(veh) | 0.2 | - | - | 0.1 | - |
| | | | | | |

Cranston, Rhode Island

Cranston Street at Western Driveway







| Int Delay, s/veh | 0.2 | | | | | |
|------------------------|------|------|------|--------------|------|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ef 👘 | | | ् | Y | |
| Traffic Vol, veh/h | 547 | 5 | 0 | 490 | 6 | 7 |
| Future Vol, veh/h | 547 | 5 | 0 | 490 | 6 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 595 | 5 | 0 | 533 | 7 | 8 |

| Major/Minor M | ajor1 | Λ | /lajor2 | 1 | Minor1 | |
|-----------------------|-------|-------|---------|-----|-----------|-------|
| Conflicting Flow All | 0 | 0 | 600 | | 1131 | 598 |
| Stage 1 | - | - | - | - | 598 | - |
| Stage 2 | - | - | - | - | 533 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 977 | - | 225 | 502 |
| Stage 1 | - | - | - | - | 549 | - |
| Stage 2 | - | - | - | - | 588 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 977 | - | 225 | 502 |
| Mov Cap-2 Maneuver | - | - | - | - | 225 | - |
| Stage 1 | - | - | - | - | 549 | - |
| Stage 2 | - | - | - | - | 588 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0 | | 16.8 | |
| HCM LOS | U | | 0 | | 10.0 C | |
| | | | | | U | |
| | | | | | | |
| Minor Lane/Major Mvmt | N | BLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 320 | - | - | 977 | - |
| HCM Lane V/C Ratio | | 0.044 | - | - | - | - |
| HCM Control Delay (s) | | 16.8 | - | - | 0 | - |
| HCM Lane LOS | | С | - | - | A | - |

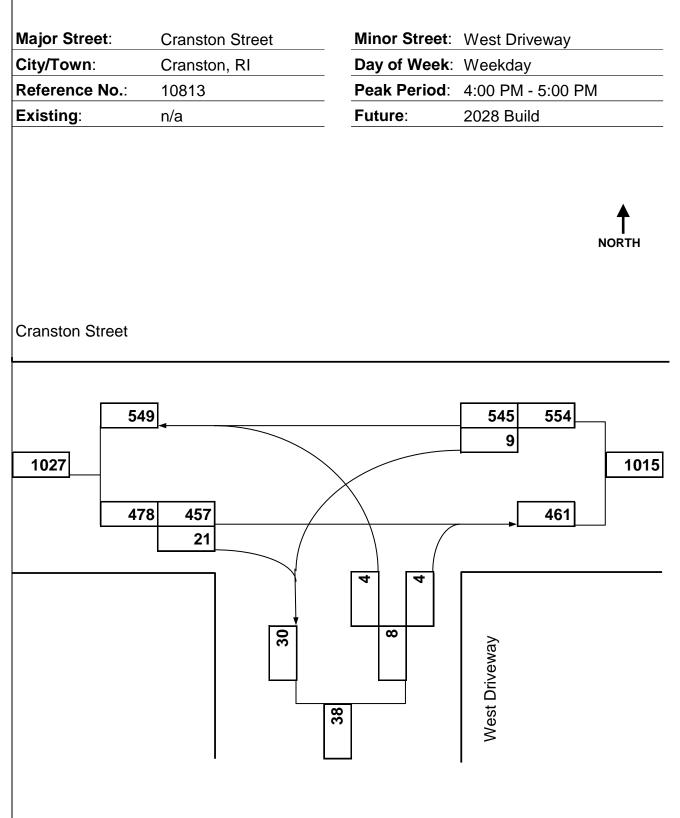
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0.1

HCM 95th %tile Q(veh)





| Int Delay, s/veh | 0.2 | | | | | |
|------------------------|------|------|------|--------------|------|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ef 👘 | | | ् | Y | |
| Traffic Vol, veh/h | 457 | 21 | 9 | 545 | 4 | 4 |
| Future Vol, veh/h | 457 | 21 | 9 | 545 | 4 | 4 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 497 | 23 | 10 | 592 | 4 | 4 |

| Major/Minor M | lajor1 | ٨ | /lajor2 | ſ | Minor1 | |
|-----------------------|--------|-------|---------|-----|-----------|-------|
| Conflicting Flow All | 0 | 0 | 520 | 0 | 1121 | 509 |
| Stage 1 | - | - | | - | 509 | - 007 |
| Stage 2 | - | - | - | - | 612 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1046 | - | 228 | 564 |
| Stage 1 | - | - | - | - | 604 | - |
| Stage 2 | - | - | - | - | 541 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1046 | - | 225 | 564 |
| Mov Cap-2 Maneuver | - | - | - | - | 225 | - |
| Stage 1 | - | - | - | - | 604 | - |
| Stage 2 | - | - | - | - | 533 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.1 | | 16.5 | |
| HCM LOS | 0 | | 0.1 | | 10.5 C | |
| | | | | | U | |
| | | | | | | |
| Minor Lane/Major Mvmt | : NI | BLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 322 | - | - | 1046 | - |
| HCM Lane V/C Ratio | C |).027 | - | - | 0.009 | - |

| HCM Lane V/C Ratio | 0.027 | - | - 0. | 009 | - | |
|-----------------------|-------|---|------|-----|---|--|
| HCM Control Delay (s) | 16.5 | - | - | 8.5 | 0 | |
| HCM Lane LOS | С | - | - | А | А | |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0 | - | |

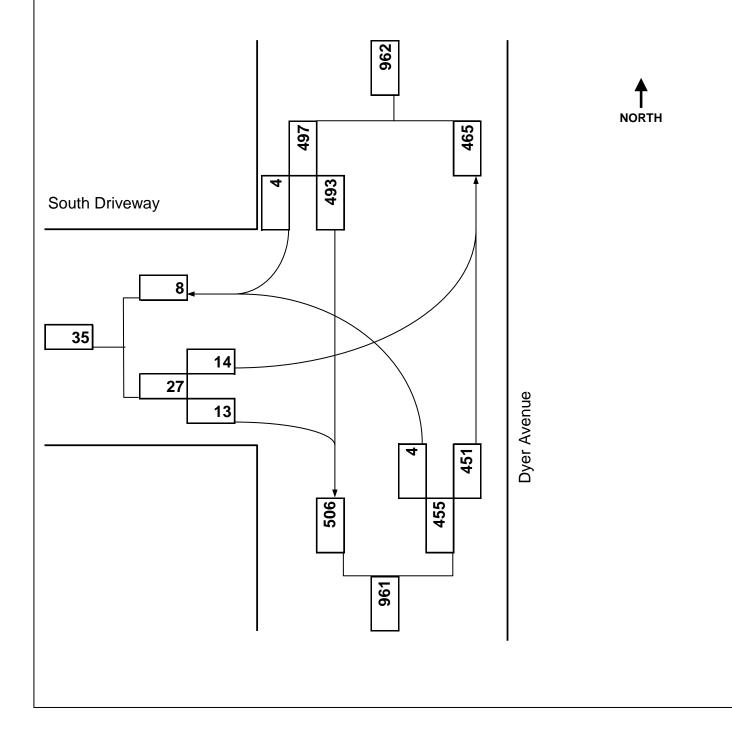
Cranston, Rhode Island

Dyer Avenue at Southern Driveway



| S | B | E | T | A |
|---|--------|--------|-------|---|
| V | /ww.Bl | ETA-In | c.com | |

| Major Street: | Dyer Avenue | Minor Street: South Driveway |
|----------------|--------------|--------------------------------|
| City/Town: | Cranston, RI | Day of Week: Weekday |
| Reference No.: | 10813 | Peak Period: 7:30 AM - 8:30 AM |
| Existing: | n/a | Future: 2028 Build |



| Int Delay, s/veh | 0.5 | | | | | | |
|------------------------|------|------|------|------------------|------|------|----------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | 1 |
| Lane Configurations | ۰¥ | | | - स ी | 4 | | |
| Traffic Vol, veh/h | 14 | 13 | 4 | 451 | 493 | 4 | ļ |
| Future Vol, veh/h | 14 | 13 | 4 | 451 | 493 | 4 | ł |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |) |
| Sign Control | Stop | Stop | Free | Free | Free | Free |) |
| RT Channelized | - | None | - | None | - | None | <u>}</u> |
| Storage Length | 0 | - | - | - | - | - | - |
| Veh in Median Storage, | ,# 0 | - | - | 0 | 0 | - | - |
| Grade, % | 0 | - | - | 0 | 0 | - | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |) |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |) |
| Mvmt Flow | 15 | 14 | 4 | 490 | 536 | 4 | ļ |

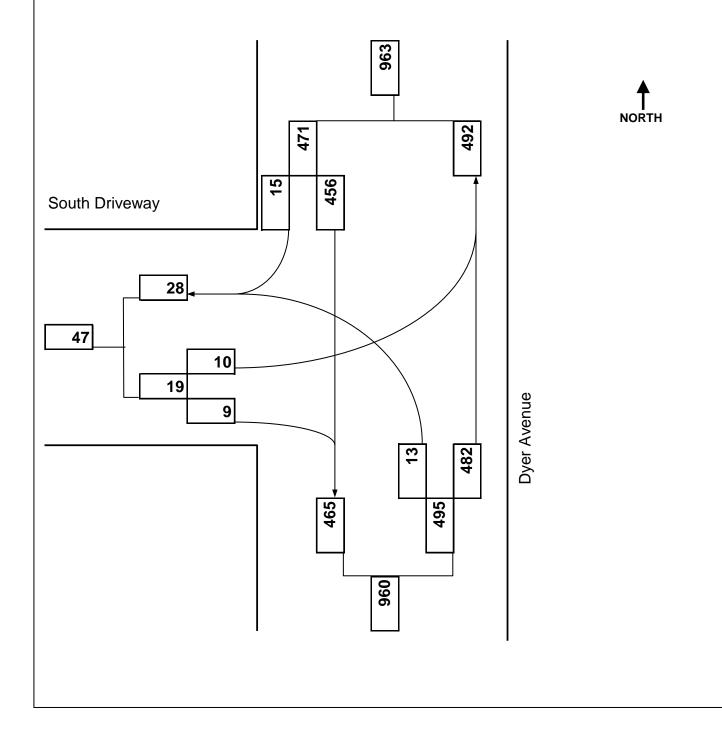
| Major/Minor | Minor2 | | Major1 | Maj | or2 | |
|----------------------|--------|-------|--------|-----|-----|---|
| Conflicting Flow All | 1036 | 538 | 540 | 0 | - | 0 |
| Stage 1 | 538 | - | - | - | - | - |
| Stage 2 | 498 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 256 | 543 | 1028 | - | - | - |
| Stage 1 | 585 | - | - | - | - | - |
| Stage 2 | 611 | - | - | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | 255 | 543 | 1028 | - | - | - |
| Mov Cap-2 Maneuver | 255 | - | - | - | - | - |
| Stage 1 | 582 | - | - | - | - | - |
| Stage 2 | 611 | - | - | - | - | - |
| | | | | | | |

| Approach | EB | NB | SB |
|----------------------|------|-----|----|
| HCM Control Delay, s | 16.5 | 0.1 | 0 |
| HCM LOS | С | | |

| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR |
|-----------------------|-------|-----|-------|-----|-----|
| Capacity (veh/h) | 1028 | - | 342 | - | - |
| HCM Lane V/C Ratio | 0.004 | - | 0.086 | - | - |
| HCM Control Delay (s) | 8.5 | 0 | 16.5 | - | - |
| HCM Lane LOS | А | А | С | - | - |
| HCM 95th %tile Q(veh) | 0 | - | 0.3 | - | - |

| | B | E | T | A |
|---|-------|--------|-------|---|
| w | ww.Bl | ETA-In | c.com | |

| Major Street: | Dyer Avenue | Minor Street: South Driveway |
|----------------|--------------|--------------------------------|
| City/Town: | Cranston, RI | Day of Week: Weekday |
| Reference No.: | 10813 | Peak Period: 4:00 PM - 5:00 PM |
| Existing: | n/a | Future: 2028 Build |



| Int Delay, s/veh | 0.4 | | | | | |
|------------------------|------|------|------|--------------|------|------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ۰¥ | | | ् | 4 | |
| Traffic Vol, veh/h | 10 | 9 | 13 | 482 | 456 | 15 |
| Future Vol, veh/h | 10 | 9 | 13 | 482 | 456 | 15 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 10 | 14 | 524 | 496 | 16 |

| Major/Minor | Minor2 |] | Major1 | Maj | or2 | | |
|----------------------|--------|-------|--------|-----|-----|---|--|
| Conflicting Flow All | 1056 | 504 | 512 | 0 | - | 0 | |
| Stage 1 | 504 | - | - | - | - | - | |
| Stage 2 | 552 | - | - | - | - | - | |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - | |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - | |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - | |
| Pot Cap-1 Maneuver | 250 | 568 | 1053 | - | - | - | |
| Stage 1 | 607 | - | - | - | - | - | |
| Stage 2 | 577 | - | - | - | - | - | |
| Platoon blocked, % | | | | - | - | - | |
| Mov Cap-1 Maneuver | | 568 | 1053 | - | - | - | |
| Mov Cap-2 Maneuver | 245 | - | - | - | - | - | |
| Stage 1 | 595 | - | - | - | - | - | |
| Stage 2 | 577 | - | - | - | - | - | |
| | | | | | | | |

| Approach | EB | NB | SB |
|----------------------|------|-----|----|
| HCM Control Delay, s | 16.5 | 0.2 | 0 |
| HCM LOS | С | | |

| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR |
|-----------------------|-------|-----|-------|-----|-----|
| Capacity (veh/h) | 1053 | - | 335 | - | - |
| HCM Lane V/C Ratio | 0.013 | - | 0.062 | - | - |
| HCM Control Delay (s) | 8.5 | 0 | 16.5 | - | - |
| HCM Lane LOS | А | А | С | - | - |
| HCM 95th %tile Q(veh) | 0 | - | 0.2 | - | - |